PHYS 5306: Classical Dynamics

Joseph D. Romano
Texas Tech University
(Fall 2022)
joseph.romano@ttu.edu

Load relevant packages

```
In[1]:= ClearAll["Global`*"]
        << Graphics`Arrow`
        << Graphics`Shapes`
        << Graphics`Polyhedra`
        << Graphics`Colors`
        << Graphics`Graphics3D`
        << Graphics`MultipleListPlot`
        << Graphics`ImplicitPlot`
        << Graphics`ParametricPlot`
        << Graphics`Legend`
        << Graphics`Animation`
        << Graphics`PlotField`
        << Graphics`PlotField3D`
        << Graphics`Spline`
        << Graphics`InequalityGraphics`
        << Graphics`FilledPlot`
        << Graphics`ComplexMap`
        << Graphics`ComplexRegion`
        << Graphics`ErrorBarPlots`
        << Graphics`ListContourPlot`
        << Graphics`ListContourPlot3D`
        << Graphics`ListPlot3D`
        << Graphics`PlotField3D`
        << Graphics`ListPlotVector3D`
        << Graphics`ParametricPlot3D`
        << Graphics`ContourPlot3D`
        << Graphics`SurfaceOfRevolution`
        << Graphics`ImplicitPlot3D`
        << Graphics`Colors`
        << Graphics`Shapes`
        << Graphics`Polyhedra`
        << Graphics`Graphics3D`
        << Graphics`MultipleListPlot`
        << Graphics`ImplicitPlot`
        << Graphics`ParametricPlot`
        << Graphics`Legend`
        << Graphics`Animation`
        << Graphics`PlotField`
        << Graphics`PlotField3D`
        << Graphics`Spline`
        << Graphics`InequalityGraphics`
        << Graphics`FilledPlot`
        << Graphics`ComplexMap`
        << Graphics`ComplexRegion`
        << Graphics`ErrorBarPlots`
        << Graphics`ListContourPlot`
        << Graphics`ListContourPlot3D`
        << Graphics`ListPlot3D`
        << Graphics`PlotField3D`
        << Graphics`ListPlotVector3D`
        << Graphics`ParametricPlot3D`
        << Graphics`ContourPlot3D`
        << Graphics`SurfaceOfRevolution`
        << Graphics`ImplicitPlot3D`
        << Graphics`Colors`
        << Graphics`Shapes`
        << Graphics`Polyhedra`
        << Graphics`Graphics3D`
        << Graphics`MultipleListPlot`
        << Graphics`ImplicitPlot`
        << Graphics`ParametricPlot`
        << Graphics`Legend`
        << Graphics`Animation`
        << Graphics`PlotField`
        << Graphics`PlotField3D`
        << Graphics`Spline`
        << Graphics`InequalityGraphics`
        << Graphics`FilledPlot`
        << Graphics`ComplexMap`
        << Graphics`ComplexRegion`
        << Graphics`ErrorBarPlots`
        << Graphics`ListContourPlot`
        << Graphics`ListContourPlot3D`
        << Graphics`ListPlot3D`
        << Graphics`PlotField3D`
        << Graphics`ListPlotVector3D`
        << Graphics`ParametricPlot3D`
        << Graphics`ContourPlot3D`
        << Graphics`SurfaceOfRevolution`
        << Graphics`ImplicitPlot3D`
```

0. Useful mathematical identities, special functions, etc.

- Review of vector calculus, calculus of variations, linear algebra, ...
- Fog identities
- Double angle formulae
- Potentials: two-body identities
- Some standard integrals
- Taylor series and binomial theorem
- Plane, cross product, and Jacobian identities

1. Lagrangian mechanics (1-5)

- Write down the Lagrangian for a simple system in terms of generalized coordinates.
- Distinguish generalized coordinates from Cartesian coordinates.
- Write down Lagrange's equations.
- Define the action in terms of the Lagrangian, and derive Lagrange's equations starting from the action.
- Show that Lagrange's equations are unchanged if we add a total time derivative $\frac{dF(q,t)}{dt}$ to L.
- Include holonomic and time-dependent constraints in the Lagrangian formalism by introducing Lagrange multipliers.
- Define and give examples of a cyclic (ignorable) coordinate and a conserved quantity.

2. Conservation laws (6-10)

- Show how conservation of energy, momentum, and angular momentum are connected to time translation, space translation, and rotational symmetry.
- Derive the Hamiltonian equations for energy, momentum, and angular momentum from one-family flows Φ_s & another Φ'.
- Write down the general expression for the energy function E.
- Explain what it means for a function to be homogeneous of degree k.
- Write down the expression for the generalized momentum p_i.
- Write down the expression for the center of mass (COM) of a system of particles.
- Write down the total linear momentum $\mathbf{P}$ of a system of particles.
- Write down the total angular momentum $\mathbf{L}$ of a system of particles.
- Write down the expression for the moment of inertia I about an axis (fixed) in a plane.
- Write down the parallel axis theorem relating the moment of inertia about a parallel axis to the moment of inertia about the COM.
- Write down the moment of inertia tensor I_{ij} for a rigid body with respect to a coordinate system.
- Write down the expression for the angular momentum vector $\mathbf{L}$ in terms I_{ij} and ω_j.
- Write down the expression for the kinetic energy T in terms of I_{ij} and ω_j.
- Write down the Euler equations for a rigid body with respect to the principal axes.
- Derive the Euler equations using Hamilton's equations of motion in the body frame.
- Derive Lagrange's equations for the motion of a rigid body.
- Calculate the components of $\mathbf{I}$ in the body frame in terms of the Euler angles and their time derivatives.
- Derive the Hamilton-Jacobi PDE for Hamilton's principle function S.

3. Central force motion (11, 13-15)

- Write down an integral expression for t in terms of r or θ if motion is a constant central force $\mathbf{f}(r)\hat{\mathbf{r}}$.
- Determine the orbital shape of the energy and turning points for k a rational or a rational multiple of π.
- Transform the problem of two interacting particles into an effective one-body problem by working in the COM frame.
- Show that total energy and angular momentum are conserved for a central potential.
- Write down an expression for the effective potential $V_{\text{eff}}(r)$ in terms of $U(r)$ and $\mathbf{M}$.
- Find the effective potential for some simple central force problem.
- Know the graph of the effective potential, determine the different types of allowed motion.
- Derive the differential equation for the orbit $u(\theta)$ in terms of $f(1/u)$ and $\mathbf{M}$.
- Prove that Kepler's third law is Kepler's problem for bound orbits and interpret the constant in the proportionality.
- Derive the relationship between E, M, a, b, c, and p for an ellipse.
- Derive the Laplace-Runge-Lenz vector $\mathbf{A}$, and show that it is a conserved quantity for Kepler's problem.
- Know and derive Kepler's three laws of planetary motion.
- Calculate the differences in θ over the elliptical, parabolic, and hyperbolic motion.

4. Collisions and scattering (16-20)

- Draw diagrams relating velocities in the lab and COM frames for the kinematics of a single particle.
- Draw diagrams relating velocities in the lab and COM frames for an elastic collision of two particles, one initially at rest in the lab frame.
- Explain what information can and cannot be determined in an elastic collision of two particles, using your conservation of momentum and kinetic energy.
- Derive the expression for the deflection angle Θ in terms of the impact parameter b.
- Write down the expression for the scattering cross section σ in terms of the impact parameter b.
- Derive the Rutherford scattering cross section σ in terms of the energy E and angle deflection Θ.
- Derive an integral expression for $\Delta\chi$ and solve it for simple potentials — e.g. $U(r) = kr$ or the Rutherford scattering.
- Write down expressions for the 4 vectors of $(p, \mathbf{p}, iE/c, \mathbf{p})$, $(E, \mathbf{p}c)$, $(E/c, \mathbf{p})$, $(E, \mathbf{p}c, mc^2)$.
- Explain how one can get an expression for the scattering angle Θ in the lab frame from the integral equation for $\Delta\chi$.

5. Small oscillations (21-23)

- Explain what stable equilibrium means in terms of the potential energy $U(q)$.
- Calculate the frequency for small oscillations about a position of stable equilibrium.
- Solve the equations of motion for both the free and forced oscillations in one dimension, noting the difference between the general solution of the homogeneous equation and a particular solution.
- Derive the Lagrangian density corresponding to the wave equation for small oscillations of systems with more than one DOF.

7. Rigid body motion (31-36, 38)

- Draw a diagram showing the body frame and fixed reference frame.
- Show that the angular velocity vector is unchanged under a shift in the origin of the body frame.
- Write down an expression for the instantaneous $\mathbf{v}_{\text{rot}}$ of the inertia tensor as a sum over discrete mass points or as an integral over the volume of the body.
- Compute the components of the inertia tensor for a rigid body with respect to a coordinate system.
- Obtain or identify the principal axes of inertia for various rigid bodies.
- Write down the expression for the angular momentum vector $\mathbf{M}$ in terms I_{ij} and ω_j.
- Write down the expression for the kinetic energy T in terms of I_{ij} and ω_j.
- Explain how to diagonalize the inertia tensor to find the principal axes of inertia.
- Derive the Euler equations for rigid bodies motion (equations of motion in the body frame).
- Derive Lagrange's equations for the motion of a rigid body.
- Calculate the components of $\mathbf{I}$ in the body frame in terms of the Euler angles and their time derivatives.
- Derive the Hamilton-Jacobi PDE for Hamilton's principle function S.

8. Non-inertial reference frames (39)

- Draw a diagram labeling an inertial and non-inertial reference frame.
- Derive the relationship between the time derivatives of a vector in the two reference frames.
- Distinguish true inertial reference forces associated with translational and rotational motion.
- Derive the Coriolis, centrifugal, transverse acceleration, and rotational acceleration fictitious forces.
- Explain the physical significance of Foucault's pendulum.

0. Useful mathematical identities, special functions, etc.

1) Review of vector calculus, etc.: https://link.springer.com/content/pdf/bbm%3A978-3-319-68780-3%2F1.pdf

2) Fog identities:

$$\begin{aligned}
\sin^2\alpha + \cos^2\alpha &= 1 \\
\sin(\beta \pm B) &= \sin\beta\cos B \pm \cos\beta\sin B \\
\cos(\beta \pm B) &= \cos\beta\cos B \mp \sin\beta\sin B \\
\tan\beta \pm B &= \frac{\tan\beta \pm \tan B}{1 \mp \tan\beta\tan B} \\
\sin\alpha - \sin\beta &= 2\sin\left(\frac{\alpha-\beta}{2}\right)\cos\left(\frac{\alpha+\beta}{2}\right) \\
\cos\alpha + \cos\beta &= 2\cos\left(\frac{\alpha-\beta}{2}\right)\cos\left(\frac{\alpha+\beta}{2}\right)
\end{aligned}$$

3) Double-angle formulae:

$$\begin{aligned}
\sin 2\alpha &= 2\sin\alpha\cos\alpha \\
\cos 2\alpha &= \cos^2\alpha - \sin^2\alpha = \frac{1-\tan^2\alpha}{1+\tan^2\alpha} \\
\tan 2\alpha &= \frac{2\tan\alpha}{1-\tan^2\alpha} \\
\sin^2\alpha &= \frac{1-\cos 2\alpha}{2}, \quad \cos^2\alpha = \frac{1+\cos 2\alpha}{2}
\end{aligned}$$

4) Hyperbolic function identities:

$$\begin{aligned}
\cosh^2\alpha - \sinh^2\alpha &= 1 \\
\sinh^{-1}(\alpha) &= \ln\left(\alpha + \sqrt{\alpha^2+1}\right) \\
\cosh^{-1}(\alpha) &= \ln\left(\alpha + \sqrt{\alpha^2-1}\right) \\
\tanh^{-1}(\alpha) &= \frac{1}{2}\ln\left(\frac{1+\alpha}{1-\alpha}\right)
\end{aligned}$$

5) Some standard integrals:

$$\begin{aligned}
\int \sin^2\alpha\, d\alpha &= \frac{\alpha}{2} - \frac{\sin 2\alpha}{4} \\
\int \cos^2\alpha\, d\alpha &= \frac{\alpha}{2} + \frac{\sin 2\alpha}{4} \\
\int \frac{d\alpha}{\sin^2\alpha} &= -\cot\alpha + \text{const} \\
\int \frac{d\alpha}{\cos^2\alpha} &= \tan\alpha + \text{const} \\
\int \frac{d\alpha}{\sqrt{1-\alpha^2}} &= \sin^{-1}\alpha + \text{const} \\
\int \frac{d\alpha}{\sqrt{\alpha^2-1}} &= \cosh^{-1}\alpha + \text{const}, \quad (\alpha > 1) \\
\int \frac{d\alpha}{1-\alpha^2} &= \tanh^{-1}\alpha + \text{const}, \quad (|\alpha| < 1) \\
\int \frac{d\alpha}{\sqrt{\alpha^2+1}} &= \sinh^{-1}\alpha + \text{const}, \quad (\alpha \geq 1)
\end{aligned}$$

6) Beta function and Gamma function:

$$B(\alpha,\beta) = \int_0^1 x^{\alpha-1}(1-x)^{\beta-1}\, dx = \frac{\Gamma(\alpha)\Gamma(\beta)}{\Gamma(\alpha+\beta)}, \quad \text{where } \mathrm{Re}(\alpha) > 0,\ \mathrm{Re}(\beta) > 0$$

$$\Gamma(z) = \int_0^\infty x^{z-1}e^{-x}\, dx, \quad \text{where } \mathrm{Re}(z) > 0$$

$\Gamma(z)$ is a generalization of the factorial function of z:

$$\Gamma(z+1) = z!\,\Gamma(z)$$

Useful value:

$$\Gamma(1/2) = \sqrt{\pi}$$

7) Elliptic functions and integrals:

Consider an ellipse with semi-major axis a, semi-minor axis b, and eccentricity $e = \sqrt{1 - \frac{b^2}{a^2}}$:

As usual let

$$x = a\cos\theta, \qquad y = a\sin\theta, \qquad x^2 + y^2 = a^2$$

For a given θ, define the following three functions

$$\begin{aligned}
\sin\theta &= \sin\theta, & \cos\theta &= \cos\theta, & \Delta\theta &= \sqrt{1 - e^2\sin^2\theta} \\
\sin\theta &= \sin\theta, & \sin(\pi - \theta) &= \sin\theta, & \Delta(\pi - \theta) &= \Delta\theta \\
\sin\theta &= -\sin\theta, & \sin(2\pi + \theta) &= \sin\theta, & \Delta(2\pi + \theta) &= \Delta\theta
\end{aligned}$$

where the argument α is defined by

$$\alpha = \int_0^\theta \Delta\theta'\, d\theta'$$

Then it's easy to show that

$$\begin{aligned}
\alpha(\pi - \theta) &= 2\alpha(\pi/2) - \alpha(\theta), & \alpha(2\pi + \theta) &= 2\alpha(\pi) + \alpha(\theta)
\end{aligned}$$

where we have dropped the θ dependence above (and henceforth) to simplify the notation.

Now we also prove the following differential identities:

$$\begin{aligned}
\frac{d\sin\theta}{d\alpha} &= \frac{d\sin\theta}{d\theta}\frac{d\theta}{d\alpha} = \frac{\cos\theta}{\Delta\theta} = \cos\theta, & \frac{d\cos\theta}{d\alpha} &= \frac{d\cos\theta}{d\theta}\frac{d\theta}{d\alpha} = -\frac{\sin\theta}{\Delta\theta} = -\sin\theta
\end{aligned}$$

These equations can be integrated (e.g. the first one)

$$\alpha = \int \frac{d\sin\theta}{\cos\theta} = \int \frac{d\sin\theta}{\sqrt{1-\sin^2\theta}} = \sin^{-1}\sin\theta, \quad \text{where } -\pi/2 \leq \theta \leq \pi/2$$

or, equivalently,

$$\sin\theta = \sin\alpha$$

This equation is typically written in mathematical handbooks as the (weird-looking) function of the first kind with amplitude θ and modulus k

$$\alpha = F(\theta, k) = \int_0^\theta \frac{d\theta'}{\sqrt{1 - k^2\sin^2\theta'}}$$

Setting $k(e) = 1$ gives the complete elliptic integral of the first kind:

$$K(k) = F(\pi/2, k) = \int_0^{\pi/2} \frac{d\theta'}{\sqrt{1 - k^2\sin^2\theta'}}$$

There are also (quite elliptic functions and complete elliptic integrals of the 2nd and 3rd kinds):

2nd kind

$$\begin{aligned}
E(\theta, k) &= \int_0^\theta \sqrt{1 - k^2\sin^2\theta'}\, d\theta', & E(k, \theta) &= \int_0^{\sin\theta} \frac{\sqrt{1-k^2x^2}}{\sqrt{1-x^2}}\, dx
\end{aligned}$$

3rd kind

$$\begin{aligned}
\Pi(n, \theta, k) &= \int_0^\theta \frac{d\theta'}{(1 + n\sin^2\theta')\sqrt{1 - k^2\sin^2\theta'}}, & \Pi(n, k) &= \int_0^{\pi/2} \frac{d\theta'}{(1 + n\sin^2\theta')\sqrt{1 - k^2\sin^2\theta'}}
\end{aligned}$$

The (quite elliptic functions and complete elliptic integrals of the 2nd and 3rd kinds) are also typically written in mathematical handbooks as the (weird-looking) functions of the first kind with amplitude θ and modulus k (NOTE: The functions $\text{sn}(\alpha, k)$, $\text{cn}(\alpha, k)$ are generalizations of the circular functions $\sin\theta$, $\cos\theta$ to ellipse with eccentricity k. When $k = 0$, $\text{sn} \to \sin$, $\text{cn} \to \cos$, and $\text{dn} \to 1$):

$$\begin{aligned}
\text{sn}(\alpha, k) &= \sin\theta, & \text{cn}(\alpha, k) &= \cos\theta, & \text{dn}(\alpha, k) &= \Delta\theta
\end{aligned}$$

The angle θ also is an elliptic function of α and k, known as the Jacobi amplitude function:

$$\theta = \text{am}(\alpha, k), \qquad \text{sn}(\alpha, k) = \sin\theta, \qquad \text{cn}(\alpha, k) = \cos\theta, \qquad \text{dn}(\alpha, k) = \Delta\theta$$

Note that α can be the same as the polar coordinate angle θ in the above (quite complicated) sense. These three functions are related by

$$\text{sn}^2(\alpha, k) + \text{cn}^2(\alpha, k) = 1, \qquad k^2\,\text{sn}^2(\alpha, k) + \text{dn}^2(\alpha, k) = 1$$

1. Lagrangian mechanics (1-5)

1) Write down the Lagrangian for a simple system in terms of generalized coordinates.

Example:

Mass generally

$$T(q,\dot{q},t) = T = T = \frac{1}{2}\sum_{i,j=1}^{3} m_i (\dot{x}_{ij} - \dot{x}_{3j})^2, \quad U(q,\dot{q},t) = U(x_1 - x_2, \ldots, x_3 - x_2)$$

for a system of particles in an inertial frame.

2) Distinguish generalized coordinates from Cartesian coordinates.

Example: Double pendulum

3) Write down Lagrange's equations.

See the first couple in 2), for the generalized coordinates q_j, as opposed to the Cartesian coordinates (x_i, y_i) and (x_j, y_j), which are subject to constraints imposed by the rigid rods of length l.

4) Define the action in terms of the Lagrangian, and derive Lagrange's equations starting from the action.

Action:

$$S[q] = \int_{t_1}^{t_2} L(q,\dot{q},t)\, dt$$

Lagrange's equations are determined by setting $\delta S = 0$ for variations that first vanish at the end points t_1 and t_2:

The following derivation is for a single degree of freedom. For multiple degrees of freedom, we can just sum over $j = 1, 2, \ldots$ independently. Derivation:

$$\delta S = \int_{t_1}^{t_2} \delta L\, dt = \int_{t_1}^{t_2} \left(\frac{\partial L}{\partial q}\delta q + \frac{\partial L}{\partial \dot{q}}\delta\dot{q} \right) dt$$

Integrate the second term by parts using

$$\delta\dot{q} = \frac{d}{dt}(\delta q) = \frac{d}{dt}\delta q$$

obtaining

$$\delta S = \int_{t_1}^{t_2} \left(\frac{\partial L}{\partial q} - \frac{d}{dt}\frac{\partial L}{\partial \dot{q}} \right) \delta q\, dt + \left. \frac{\partial L}{\partial \dot{q}}\delta q \right|_{t_1}^{t_2}$$

The last term below vanish given the condition that the variations δq vanish at the end points. Setting $\delta S = 0$ is equivalent to the integrand vanishing:

$$\frac{\partial L}{\partial q} - \frac{d}{dt}\frac{\partial L}{\partial \dot{q}} = 0$$

5) Show that Lagrange's equations are unchanged if one adds a total time derivative $\frac{dF(q,t)}{dt}$ to L.

Define

$$L'(q,\dot{q},t) = L(q,\dot{q},t) + \frac{dF(q,t)}{dt}$$

Then

$$\begin{aligned}
S'[q] &= \int_{t_1}^{t_2} L'(q,\dot{q},t)\, dt \\
&= \int_{t_1}^{t_2} L(q,\dot{q},t)\, dt + \int_{t_1}^{t_2} \frac{dF(q,t)}{dt}\, dt \\
&= S[q] + F(q(t_2), t_2) - F(q(t_1), t_1)
\end{aligned}$$

From this we see that $\delta S' = \delta S$ since $\delta q = 0$ at t_1 and t_2, by the limits the 2 and $\delta S = 0$ gives $\delta S' = 0$ as the same time.

Here we can also start with the result for working directly with the generalized coordinates q_i and $\dot{q}_i$:

$$\begin{aligned}
\frac{\partial L'}{\partial q_i} &= \frac{\partial L}{\partial q_i} + \frac{\partial}{\partial q_i}\frac{dF}{dt} = \frac{\partial L}{\partial q_i} + \frac{\partial}{\partial q_i}\left(\frac{\partial F}{\partial q_j}\dot{q}_j + \frac{\partial F}{\partial t} \right) = \frac{\partial L}{\partial q_i} + \frac{\partial^2 F}{\partial q_i \partial q_j}\dot{q}_j + \frac{\partial^2 F}{\partial q_i \partial t} \\
\frac{\partial L'}{\partial \dot{q}_i} &= \frac{\partial L}{\partial \dot{q}_i} + \frac{\partial}{\partial \dot{q}_i}\frac{dF}{dt} = \frac{\partial L}{\partial \dot{q}_i} + \frac{\partial}{\partial \dot{q}_i}\left(\frac{\partial F}{\partial q_j}\dot{q}_j + \frac{\partial F}{\partial t} \right) = \frac{\partial L}{\partial \dot{q}_i} + \frac{\partial F}{\partial q_i} \\
\frac{d}{dt}\frac{\partial L'}{\partial \dot{q}_i} &= \frac{d}{dt}\frac{\partial L}{\partial \dot{q}_i} + \frac{d}{dt}\frac{\partial F}{\partial q_i} = \frac{d}{dt}\frac{\partial L}{\partial \dot{q}_i} + \frac{\partial^2 F}{\partial q_i \partial q_j}\dot{q}_j + \frac{\partial^2 F}{\partial q_i \partial t}
\end{aligned}$$

Then

$$\frac{\partial L'}{\partial q_i} - \frac{d}{dt}\frac{\partial L'}{\partial \dot{q}_i} = \frac{\partial L}{\partial q_i} - \frac{d}{dt}\frac{\partial L}{\partial \dot{q}_i}$$

6) Include holonomic and non-holonomic constraint forces in the Lagrangian formalism by introducing Lagrange multipliers.

In holonomic constraints are relationships between the generalized coordinates and possibly time:

$$\phi_j(q,t) = 0, \qquad j = 1, 2, \ldots, n - s$$

Non-holonomic constraints are relationships between the generalized coordinates and velocities:

$$\sum_{i=1}^{n} a_{ji}\dot{q}_i + a_{jt} = 0, \qquad j = 1, 2, \ldots, n - s$$

where a labels the different constraints. Holonomic constraints can be considered as a special case by setting to the Lagrange term of the form $\sum_i \lambda_j a_{ji} \dot{q}_i$ where λ_j and a_{ji} are the Lagrange multipliers. The modified equations of motion are

$$\frac{\partial L}{\partial q_i} - \frac{d}{dt}\frac{\partial L}{\partial \dot{q}_i} = \sum_{j=1}^{n-s} \lambda_j a_{ji}, \qquad i = 1, 2, \ldots, n$$

Together with the constraint equations, there are $n - s$ equations for the $n + s$ unknowns q_i and λ_j. Note that the generalized constraint force $\sum_j \lambda_j a_{ji} \equiv Q_i$ is orthogonal to the surface $\phi_j = 0$.

For the holonomic constraints we substitute between the coordinates q_i and $\dot{q}_i$ to obtain

$$\frac{\partial L}{\partial q_i} - \frac{d}{dt}\frac{\partial L}{\partial \dot{q}_i} = \sum_{j=1}^{n-s} \lambda_j \frac{\partial \phi_j}{\partial q_i}, \qquad i = 1, 2, \ldots, n$$

that could be integrated to yield relations between just the generalized coordinates q_i. The constraint constants are not included in the Lagrange formalism at the level of the equations of motion, but can be determined from the forces of constraint:

$$Q_i = \sum_{j=1}^{n-s} \lambda_j \frac{\partial \phi_j}{\partial q_i} = \sum_{j=1}^{n-s} \lambda_j a_{ji}, \qquad i = 1, 2, \ldots, n$$

where $\mathbf{Q}$ is the velocity of the COM of the sphere of radius $\sqrt{\mathbf{R}}$ in the angular velocity vector $\boldsymbol{\omega}$ and $\mathbf{r}$ is the position vector normal to the surface.

7) Define and give examples of a closed system, constant external field, and uniform field.

A closed system is isolated from it's surroundings in the sense that neither matter nor energy can be exchanged.

A (scalar) external field: The potential $U = U(\mathbf{r}, t)$, $\mathbf{r} = (x, y, z)$ has no explicit time-dependence.

A uniform field: The potential $U = -\sum_{i=1}^{n} \mathbf{F}_i \cdot \mathbf{r}_i$ is the same for all $\mathbf{r}_i$ (i.e. no explicit $\mathbf{r}_i$ dependence).

2. Conservation laws (6-10)

1) Show how conservation of energy, momentum, and angular momentum are connected to time translation, space translation, and rotational symmetry, respectively.

Summary of the Lagrangian means that $\mathbf{r}_i \to \mathbf{r}_i$ under a transformation of time, space, ...

a) Time-evolution symmetry

$$t \to t + \Delta t$$

for which

$$\frac{\partial L}{\partial t} = 0$$

Then $\frac{dE}{dt} = 0$ for all $\mathbf{r}_i$ implies

$$\frac{dE}{dt} = \sum_{i=1}^{n} \frac{\partial L}{\partial \mathbf{r}_i}\cdot\dot{\mathbf{r}}_i + \sum_{i=1}^{n} \frac{\partial L}{\partial \dot{\mathbf{r}}_i}\cdot\ddot{\mathbf{r}}_i - \frac{dL}{dt} = 0$$

Using Lagrange's equation, we can replace $\frac{\partial L}{\partial \mathbf{r}_i}$ by $\frac{d}{dt}\frac{\partial L}{\partial \dot{\mathbf{r}}_i}$ to obtain

$$\frac{dE}{dt} = \sum_{i=1}^{n} \frac{d}{dt}\frac{\partial L}{\partial \dot{\mathbf{r}}_i}\cdot\dot{\mathbf{r}}_i + \sum_{i=1}^{n} \frac{\partial L}{\partial \dot{\mathbf{r}}_i}\cdot\ddot{\mathbf{r}}_i - \frac{dL}{dt} = 0$$

Thus,

$$E = \sum_{i=1}^{n} \frac{\partial L}{\partial \dot{\mathbf{r}}_i}\cdot\dot{\mathbf{r}}_i - L = \text{const}$$

b) Space translation symmetry

$$\mathbf{r}_i \to \mathbf{r}_i + \Delta\mathbf{r}$$

for which

$$\frac{\partial L}{\partial \mathbf{r}_i} = 0$$

Then $\frac{d\mathbf{P}}{dt} = 0$ for all $\mathbf{r}_i$ implies

$$\frac{d\mathbf{P}}{dt} = \sum_{i=1}^{n} \frac{\partial L}{\partial \mathbf{r}_i} + \sum_{i=1}^{n} \frac{d}{dt}\frac{\partial L}{\partial \dot{\mathbf{r}}_i} = \sum_{i=1}^{n} \frac{d}{dt}\frac{\partial L}{\partial \dot{\mathbf{r}}_i} = 0$$

Thus,

$$\mathbf{P} = \sum_{i=1}^{n} \frac{\partial L}{\partial \dot{\mathbf{r}}_i} = \text{const}$$

This is conservation of total linear momentum.

c) Rotational symmetry

$$\mathbf{r}_i \to \mathbf{r}_i + \Delta\mathbf{r}_i, \qquad \mathbf{r}_i \to \mathbf{r}_i + \Delta\theta\,\hat{\mathbf{n}} \times \mathbf{r}_i$$

for which

$$L = L\left[\sum_i (\mathbf{r}_i + \Delta\theta\,\hat{\mathbf{n}} \times \mathbf{r}_i), \sum_i (\dot{\mathbf{r}}_i + \Delta\theta\,\hat{\mathbf{n}} \times \dot{\mathbf{r}}_i), t\right] = L\left[\sum_i \mathbf{r}_i, \sum_i \dot{\mathbf{r}}_i, t\right] + \Delta\theta\,\hat{\mathbf{n}} \cdot \sum_i \left(\frac{\partial L}{\partial \mathbf{r}_i} \times \mathbf{r}_i + \frac{\partial L}{\partial \dot{\mathbf{r}}_i} \times \dot{\mathbf{r}}_i \right)$$

Then $\frac{dL}{dt} = 0$ for all $\hat{\mathbf{n}}$ implies

$$\frac{dL}{dt} = \hat{\mathbf{n}} \cdot \sum_{i=1}^{n} \left(\frac{\partial L}{\partial \mathbf{r}_i} \times \mathbf{r}_i + \frac{\partial L}{\partial \dot{\mathbf{r}}_i} \times \dot{\mathbf{r}}_i \right) = 0$$

Thus,

$$\mathbf{M} = \sum_{i=1}^{n} \mathbf{r}_i \times \frac{\partial L}{\partial \dot{\mathbf{r}}_i} = \sum_{i=1}^{n} \mathbf{r}_i \times \mathbf{p}_i = \text{const}$$

This is conservation of total angular momentum.

2) Derive the transformation equations for energy, momentum, and angular momentum from one inertial frame K to another K'.

Two inertial frames K and K' are related by a constant velocity $\mathbf{v}$. K' is at rest in the unprimed frame and the rest of the two coordinate systems coincide at the instant under consideration, so that the position vectors $\mathbf{r}_i$ and $\mathbf{r}'_i$ of mass point m_i are for the two inertial frames agree.

The velocities $\mathbf{u}_i$ and $\mathbf{u}'_i$ of the mass point m_i are related by

$$\mathbf{r}_i = \mathbf{r}'_i + \mathbf{v}t$$

Energy:

$$E = \frac{1}{2}\sum_i m_i u_i^2 = \frac{1}{2}\sum_i m_i (\mathbf{u}'_i + \mathbf{v})^2 = \frac{1}{2}\sum_i m_i u_i'^2 + \mathbf{v}\cdot\sum_i m_i \mathbf{u}'_i + \frac{1}{2}v^2\sum_i m_i$$

Now

$$\sum_i m_i \mathbf{u}'_i = \sum_i m_i \frac{d\mathbf{r}'_i}{dt} = \frac{d}{dt}\sum_i m_i \mathbf{r}'_i = \frac{d}{dt}(M\mathbf{R}' + M\mathbf{V}t) = M\mathbf{V}$$

where $\mathbf{r}'_i = \sum_i m_i \mathbf{r}'_i$ is the total mass, and $M\mathbf{R}' = \sum_i m_i \mathbf{r}'_i$ is by the second time derivative is the COM. Thus

$$E = \frac{1}{2}\sum_i m_i u_i'^2 + \mathbf{v}\cdot M\mathbf{V} + \frac{1}{2}Mv^2$$

Momentum:

$$\mathbf{P} = \sum_i m_i \mathbf{u}_i = \sum_i m_i (\mathbf{u}'_i + \mathbf{v}) = \mathbf{P}' + M\mathbf{v}$$

Angular momentum:

$$\mathbf{M} = \sum_i m_i \mathbf{r}_i \times \mathbf{u}_i = \sum_i m_i (\mathbf{r}'_i + \mathbf{v}t) \times (\mathbf{u}'_i + \mathbf{v}) = \mathbf{M}' + \mathbf{R}' \times M\mathbf{v} + M\mathbf{V}t \times \mathbf{v}$$

In summary

$$\begin{aligned}
E &= E' + \mathbf{v}\cdot\mathbf{P}' + \frac{1}{2}Mv^2, & \mathbf{P} &= \mathbf{P}' + M\mathbf{v}, & \mathbf{M} &= \mathbf{M}' + \mathbf{R}' \times M\mathbf{v}
\end{aligned}$$

3) Write down the general expression for the energy function E.

$$E = \sum_{i=1}^{n} \frac{\partial L}{\partial \dot{q}_i}\dot{q}_i - L$$

4) Explain what it means for a function to be homogeneous of degree k.

A function $f(x_1, x_2, \ldots)$ is homogeneous of degree k if

$$f(\alpha x_1, \alpha x_2, \ldots) = \alpha^k f(x_1, x_2, \ldots)$$

For such a function

$$x_1\frac{\partial f}{\partial x_1} + x_2\frac{\partial f}{\partial x_2} + \cdots = kf(x_1, x_2, \ldots)$$

which can be proved by differentiating both sides of the first equation with respect to α, and then evaluating at $\alpha = 1$.

Example: the kinetic energy

$$T = \frac{1}{2}\sum_{i=1}^{n} m_i \dot{x}_i^2$$

is homogeneous of degree 2 in the generalized velocities $\dot{q}_i$, so that

$$\sum_{i=1}^{n} \dot{q}_i \frac{\partial T}{\partial \dot{q}_i} = 2T$$

5) Write down the expression for the generalized momentum p_i.

$$p_i = \frac{\partial L}{\partial \dot{q}_i}, \qquad i = 1, 2, \ldots, n$$

6) Write down the expression for the center of mass (COM) of a system of particles.

$$\mathbf{R} = \frac{\sum_i m_i \mathbf{r}_i}{\sum_i m_i}$$

7) Write down the total linear momentum $\mathbf{P}$ of a system of particles.

$$\mathbf{P} = \sum_i m_i \dot{\mathbf{r}}_i$$

which implies

$$\mathbf{P} = \frac{d(M\mathbf{R})}{dt} = M\dot{\mathbf{R}} = M\mathbf{V}$$

More generally, for a potential that is homogeneous of degree k

$$U(\lambda\mathbf{r}_1, \lambda\mathbf{r}_2, \ldots) = \lambda^k U(\mathbf{r}_1, \mathbf{r}_2, \ldots)$$

where angle brackets means time average

$$\langle T \rangle = \frac{k}{2}\langle U \rangle$$

For Newtonian gravity, the potential $U = -GMm/r$ is homogeneous of degree $k = -1$.

Proof:

If T is homogeneous of degree 2, then

$$\sum_{i=1}^{n} \dot{q}_i \frac{\partial T}{\partial \dot{q}_i} = 2T$$

The LHS of the above equation can be written as

$$\sum_{i=1}^{n} \dot{q}_i \frac{\partial T}{\partial \dot{q}_i} = \sum_{i=1}^{n} \dot{q}_i \frac{\partial L}{\partial \dot{q}_i} = \sum_{i=1}^{n} \dot{q}_i p_i$$

where the first equality follows from Lagrange's equations and the second equality follows from the definition of p_i. Thus,

$$\sum_{i=1}^{n} \dot{q}_i p_i = 2T$$

The last term equals twice the kinetic energy T since $p_i = m_i\dot{q}_i$, and the first term vanishes if we take the time average, assuming that the motion is bounded (i.e., finite velocities and finite distances). Thus,

$$\langle T \rangle = \frac{k}{2}\langle U \rangle$$

3. Hamiltonian mechanics (40)

1) Write down the Hamiltonian $H(p,q,t)$ for a simple system starting from a Lagrangian $L(q,\dot{q},t)$.

General relationship:

$$\dot{q}_i(q,p,t) = \dot{q}_i(q,p,t)$$

where on the RHS all of the $\dot{q}_i$ are expressed in terms of q, p, and t.

Legendre

$$h(u,v) = \sum_i u_i v_i - f(u,v)$$

Then

$$u \to \frac{\partial f}{\partial v} = w \qquad v \to \frac{\partial f}{\partial u} = z$$

leading to

$$\frac{\partial h}{\partial u_i} = v_i$$

2) Write down Hamilton's equations for p_i and q_i.

Follow

$$\begin{aligned}
\dot{q}_i &= \frac{\partial H}{\partial p_i} \\
\dot{p}_i &= -\frac{\partial H}{\partial q_i}
\end{aligned}$$

3) Explain the fundamental difference between Hamilton's equations and Lagrange's equations.

Hamilton's equations are of the form of first-order differential equations (e.g., while Lagrange's equations are in general second-order equations).

4) Derive Hamilton's equations from Hamilton's principle.

Hamilton's principle is that the action integral

$$S = \int_{t_1}^{t_2} L(q,\dot{q},t)\, dt$$

for the actual path of motion is stationary (i.e., $\delta S = 0$) for small variations in

Lagrangian equations:

$$\frac{d}{dt}\left(\frac{\partial L}{\partial \dot{q}_i}\right) - \frac{\partial L}{\partial q_i} = 0 \quad \text{and} \quad \dot{r} = \frac{dr}{dt}$$

Hamilton's equations

$$\frac{dq_i}{dt} = \frac{\partial H}{\partial p_i} \quad \text{and} \quad \frac{dp_i}{dt} = -\frac{\partial H}{\partial q_i}$$

Solving the first of Hamilton's equations for p_i and then substituting the solution into the second equation yields

$$m\ddot{q}_i = -\frac{\partial H}{\partial q_i}$$

which is the same as Lagrange's equation.

4. Central force motion (11, 13-15)

1) Write down an integral expression for t in terms of r for 1-d motion in a constant external field $U(r)$.

Conservation of energy:

$$\frac{1}{2}m\dot{r}^2 + U(r) = E$$

where E is a constant. This is a separable differential equation with

$$t = \int \frac{dr}{\sqrt{\frac{2}{m}(E - U(r))}} + \text{const}$$

2) Determine the allowed values of the energy and turning points for 1-d motion in a constant external field.

Allowed values of the energy:

$$E \geq U_{\min}$$

since kinetic energy is positive.

Turning points are solutions to the equation $E - U(x) = 0$.

3) Transform the problem of two interacting particles into an effective one-body problem by working in the COM frame.

Lagrangian for two interacting particles:

$$L = \frac{1}{2}m_1\dot{r}_1^2 + \frac{1}{2}m_2\dot{r}_2^2 - U(|r_2 - r_1|)$$

Total kinetician is conserved since L is unchanged by a spatial translation $r_i \to r_i + \delta a$. Thus, we can work in the COM frame where the COM is the origin of coordinates:

$$r_1 m_1 + r_2 m_2 = 0$$

In terms of the relative separation vector

$$r = r_2 - r_1$$

we have

$$r_1 = -\frac{m_2}{m_1 + m_2} r \qquad r_2 = \frac{m_1}{m_1 + m_2} r$$

The kinetic energy becomes

$$\frac{1}{2}m_1\dot{r}_1^2 + \frac{1}{2}m_2\dot{r}_2^2 = \frac{1}{2}\mu\dot{r}^2$$

where

$$\mu = \frac{m_1 m_2}{m_1 + m_2}$$

is the reduced mass. Thus,

$$L = \frac{1}{2}\mu\dot{r}^2 - U(r)$$

4) Show that both energy and angular momentum are conserved for a central potential.

For a central potential, U depends only on the magnitude of the relative separation vector

$$U = U(|r_2 - r_1|) = U(r)$$

Energy:

$$E = \frac{\partial L}{\partial \dot{r}}\dot{r} - L = \frac{1}{2}\mu\dot{r}^2 + U(r)$$

is conserved since the Lagrangian does not depend explicitly on time.

Angular momentum:

$$M = r \times p = r \times \mu\dot{r}$$

$$\dot{r} \times r = 0 = r \times \dot{r} \quad \Rightarrow \quad \dot{r} \times r = 0 = r \times \dot{r}$$

Since M is constant, we can choose the orientation of our COM frame such that M points along the z-axis. Then the motion is in the xy-plane and we can write the Lagrangian in terms of plane polar coordinates (r, ϕ) and find the derivatives

$$L = \frac{1}{2}\mu(\dot{r}^2 + r^2\dot{\phi}^2) - U(r)$$

Conservation of angular momentum then manifests itself as conservation of

$$p_\phi = \frac{\partial L}{\partial \dot{\phi}}$$

since L does not depend explicitly on ϕ. Taking the derivative, we have

$$p_\phi = \mu r^2 \dot{\phi} \equiv M = \text{const}$$

or, equivalently,

$$\dot{\phi} = \frac{M}{\mu r^2}$$

5) Write down an expression for the effective potential $U_{\text{eff}}(r)$ in terms of $U(r)$ and ℓ.

Energy:

$$E = \frac{1}{2}\mu\dot{r}^2 + U_{\text{eff}}(r) = \frac{1}{2}\mu\dot{r}^2 + \frac{M^2}{2\mu r^2} + U(r) = \frac{1}{2}\mu\dot{r}^2 + U_{\text{eff}}(r)$$

with

$$U_{\text{eff}}(r) = \frac{M^2}{2\mu r^2} + U(r)$$

6) Plot the effective potential for some simple central force potentials.

You can find my analysis plots for the three examples:

- Newtonian gravity $U = -\alpha/r$
- Simple harmonic oscillator $U = \alpha r^2$
- General relativity $U = -\alpha/r + \beta/r^2$

```
# -*- coding: utf-8 -*-
"""
Created on Tue Oct 13 13:08:57 2020
Problem 6: Plot effective potential for Newtonian gravity
@author: Nathaniel Stenzel
"""
import numpy as np
import matplotlib.pyplot as plt
plt.rcParams.update({'font.size': 14})
plt.rcParams['figure.dpi'] = 200
plt.rcParams['savefig.dpi'] = 200
plt.rcParams['figure.figsize'] = [6, 4]
plt.rcParams['figure.facecolor'] = 'white'
plt.rcParams['figure.edgecolor'] = 'white'
plt.rcParams['figure.constrained_layout.use'] = True
plt.rcParams['figure.autolayout'] = False
plt.rcParams['savefig.facecolor'] = 'white'
plt.rcParams['savefig.edgecolor'] = 'white'
plt.rcParams['savefig.transparent'] = False
plt.rcParams['savefig.bbox'] = 'tight'
plt.rcParams['savefig.pad_inches'] = 0.1
plt.rcParams['figure.constrained_layout.h_pad'] = 0.1
plt.rcParams['figure.constrained_layout.w_pad'] = 0.1
plt.rcParams['figure.constrained_layout.hspace'] = 0.1
plt.rcParams['figure.constrained_layout.wspace'] = 0.1
plt.rcParams['figure.constrained_layout.frameon'] = False
plt.rcParams['figure.constrained_layout.compress'] = False
plt.rcParams['figure.constrained_layout.parent_pad'] = 0.1
plt.rcParams['figure.constrained_layout.nrows'] = 1
plt.rcParams['figure.constrained_layout.ncols'] = 1
plt.rcParams['figure.constrained_layout.renderer_pad'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_hspace'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_wspace'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_frameon'] = False
plt.rcParams['figure.constrained_layout.renderer_compress'] = False
plt.rcParams['figure.constrained_layout.renderer_parent_pad'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_nrows'] = 1
plt.rcParams['figure.constrained_layout.renderer_ncols'] = 1
plt.rcParams['figure.constrained_layout.renderer_renderer_pad'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_hspace'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_wspace'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_frameon'] = False
plt.rcParams['figure.constrained_layout.renderer_renderer_compress'] = False
plt.rcParams['figure.constrained_layout.renderer_renderer_parent_pad'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_nrows'] = 1
plt.rcParams['figure.constrained_layout.renderer_renderer_ncols'] = 1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_pad'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_hspace'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_wspace'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_frameon'] = False
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_compress'] = False
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_parent_pad'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_nrows'] = 1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_ncols'] = 1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_pad'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_hspace'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_wspace'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_frameon'] = False
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_compress'] = False
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_parent_pad'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_nrows'] = 1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_ncols'] = 1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_pad'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_hspace'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_wspace'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_frameon'] = False
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_compress'] = False
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_parent_pad'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_nrows'] = 1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_ncols'] = 1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_pad'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_hspace'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_wspace'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_frameon'] = False
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_compress'] = False
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_parent_pad'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_nrows'] = 1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_ncols'] = 1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_pad'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_hspace'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_wspace'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_frameon'] = False
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_compress'] = False
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_parent_pad'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_nrows'] = 1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_ncols'] = 1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_pad'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_hspace'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_wspace'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_frameon'] = False
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_compress'] = False
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_parent_pad'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_nrows'] = 1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_ncols'] = 1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_pad'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_hspace'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_wspace'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_frameon'] = False
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_compress'] = False
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_parent_pad'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_nrows'] = 1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_ncols'] = 1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_pad'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_hspace'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_wspace'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_frameon'] = False
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_compress'] = False
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_parent_pad'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_nrows'] = 1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_ncols'] = 1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_pad'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_hspace'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_wspace'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_frameon'] = False
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_compress'] = False
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_parent_pad'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_nrows'] = 1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_ncols'] = 1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_pad'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_hspace'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_wspace'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_frameon'] = False
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_compress'] = False
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_parent_pad'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_nrows'] = 1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_ncols'] = 1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_pad'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_hspace'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_wspace'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_frameon'] = False
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_compress'] = False
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_parent_pad'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_nrows'] = 1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_ncols'] = 1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_pad'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_hspace'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_wspace'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_frameon'] = False
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_compress'] = False
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_parent_pad'] = 0.1
plt.rcParams['figure.constrained_layout.renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_renderer_nrows'] = 1
plt.rcParams['figure.constrained_layout.renderer_
```

Code by: ✓ Ilia, ✓ I.B. $\qquad$ $\mathbf{m_1 = m_2 = 1}$ $\qquad$ $\mathbf{m_3 = 2}$

Code by: ✓ Ilia, ✓ I.B. $\qquad$ $\mathbf{m_1 = m_2 = 1}$ $\qquad$ $\mathbf{m_3 = 2}$

Conservation of momentum can be found.

In the CDM frame, the total momentum is zero, since the momentum of the two identical equal particles after the collision

$$\mathbf{p}_{1,2} = m\mathbf{v}_{1,2} - m\mathbf{v}_{1,2}$$

Elastic collision: The magnitude of the relative velocity vector is the same before and after the collision, $v = v'$.

For the case where $m_3 \to \infty$ body A: $v_3 \to 0$, so that $v = v_1$. Thus,

$$v_1 v' = \frac{m_1 - m_2}{m_1 + m_2} v_1 \quad \Rightarrow \quad \frac{m_1 - m_2}{m_1 + m_2} = 1$$

so B has an infinite mass.

For the case, $m_1 = m_2$, we can also find forward scattering of the particles in the frame S, $\theta_1 = \pi/2$.

Q: Explain what conservation can and cannot be obtained for an elastic collision of two particles, using just conservation of momentum and kinetic energy.

An elastic collision of two particles is mostly simply analyzed in the CDM frame. In this frame, the momentum of the two particles both before and after the collision are equal in magnitude and opposite in direction. Conservation of energy then requires that the magnitude of the relative velocity vector is unchanged by the collision:

$$\mathbf{v} = \frac{m_1 \mathbf{v}_1 + m_2 \mathbf{v}_2}{m_1 + m_2} \quad \Rightarrow \quad \mathbf{v}_1 + \mathbf{v}_2 = \mathbf{v}_1' + \mathbf{v}_2' \quad \Rightarrow \quad \mathbf{v} - \mathbf{v}_1 = \mathbf{v}_2' - \mathbf{v}$$

Hence an elastic collision can only change the direction of relative velocity vector. The direction can be determined, if, as desired by us, in the above figure.

Q: Derive formulas relating the scattering angles χ_1, χ_2 in the CDM and lab frames.

From either of the two last figures, we see that

$$\chi = 2\theta_1 = \pi \quad \text{(Cross-laserlike triangle CDM')}$$

so

$$\boxed{\theta_1 = \frac{\chi}{2} = \frac{\pi}{2}}$$

Also

$$\tan\theta_2 = \frac{\sin\chi_2}{\cos\chi_2 + \frac{m_1}{m_2}}$$

Using

$$m = \frac{m_1 m_2}{m_1 + m_2} \quad \Rightarrow \quad \frac{m}{m_1} = \frac{m_2}{m_1 + m_2} \quad \Rightarrow \quad \frac{m}{m_2} = \frac{m_1}{m_1 + m_2}$$

where the last two results hold since $m_1 = m_2$ it follows that

$$\boxed{\tan\theta_2 = \frac{\sin\chi_2}{\cos\chi_2 + 1} = \frac{2\sin\frac{\chi_2}{2}\cos\frac{\chi_2}{2}}{2\cos^2\frac{\chi_2}{2}} = \tan\frac{\chi_2}{2}}$$

For differential cross section calculations (see below), it is more convenient to rent these equations for χ in terms of θ_2 and θ_2,

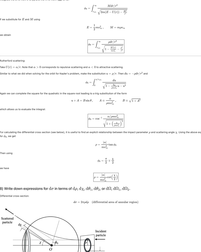
$$\cos\chi = \left(\frac{2m}{m_1}\right)\cos^2\theta_1 + \sin^2\theta_1 = \left(\frac{2m}{m_2}\right)\cos^2\theta_2$$

and

$$\chi = 2\theta_2$$

in the above equation for cos χ in terms of θ_1, we should take the + sign for $m_1 > m_2$ in order that $\chi = 0$ corresponds to $\theta_1 = 0$ for $m_1 > m_2$, both signs are necessary, indicating that for $m_1 = m_2$ we can have χ of any angle value at θ_1.

Q: Draw diagrams showing how the scattering angle χ is related to the angle of closest approach ϕ_m.



For repulsive scattering,

$$\chi + 2\alpha = \pi$$

For attractive scattering,

$$\chi + (2\alpha - \pi) = 2\alpha - \chi = \pi$$

Both of these relations can be captured by

$$\chi = |\pi - 2\alpha|$$

Q: Relate the impact parameter ρ and initial velocity v_∞ to the energy E and angular momentum M.

Solution:

$$E = \frac{1}{2}mv_\infty^2, \quad M = mv\rho_\infty$$

where in the delayed mass of the system is $m = m_1 m_2/(m_1 + m_2)$.

Q: Derive an integral expression for ϕ_m and solve it for simple potentials—e.g., $U(r) = -\alpha/r$ for Rutherford scattering.

Start with the central force differential equation for ϕ

$$d\phi = \frac{M dr/r^2}{\sqrt{2m(E - U(r)) - M^2/r^2}}$$

Integrate the LHS from 0 to ϕ_m and the RHS from r_{min} to ∞:

$$\phi_m = \int_{r_{min}}^{\infty} \frac{M dr/r^2}{\sqrt{2m(E - U(r)) - M^2/r^2}}$$

If we substitute for E and M using

$$E = \frac{1}{2}mv_\infty^2, \quad M = mv\rho_\infty$$

we obtain

$$\boxed{\phi_m = \int_{r_{min}}^{\infty} \frac{\rho dr/r^2}{\sqrt{1 - U(r)/E - \rho^2/r^2}}}$$

Rutherford scattering:

Take $U(r) = \alpha/r$. Note that $\alpha > 0$ corresponds to repulsive scattering and $\alpha < 0$ to attractive scattering.

Solve to start we will when solving for the turn the integral variable, take the substitution $u = \rho/r$. Then $du = -\rho dr/r^2$ and

$$\phi_m = \int_0^{u_{max}} \frac{du}{\sqrt{1 - \frac{2m\alpha}{E\rho}u - u^2}} = \int_0^{u_{max}} \frac{du}{\sqrt{1 - \frac{\alpha}{\rho v_\infty^2}u - u^2}}$$

Again we complicate the square for the quadratic in the square root leading to a big substitution of the form

$$u = A\sin\theta, \quad A = \frac{\alpha}{\rho v_\infty^2}, \quad B = \frac{\alpha^2}{\rho^2 v_\infty^4} + 1$$

which allows us to evaluate the integral

$$\phi_m = \int_{\sin^{-1}\left(\frac{\alpha}{\rho v_\infty^2}\right)}^{\pi/2} \frac{A\cos\theta d\theta}{\sqrt{1 - A^2\sin^2\theta - A\sin\theta}} = \int_{\sin^{-1}\left(\frac{\alpha}{\rho v_\infty^2}\right)}^{\pi/2} \frac{d\theta}{\sqrt{1 + \frac{\alpha}{\rho v_\infty^2}\sin\theta}}$$

For calculating the differential cross section (see below), it is useful to find an explicit relationship between the impact parameter ρ and scattering angle χ using the above expression for ϕ_m as get

$$\chi = \pi - 2\phi_m$$

Then using

$$\phi_m = \frac{\pi}{2} - \frac{\chi}{2}$$

we have

$$\boxed{\rho = \frac{\alpha}{m v_\infty^2}\cot\frac{\chi}{2}}$$

Q: Write down expressions for Ω in terms of ϕ_0, ϕ_f, $\Delta\theta_1$, $\Delta\theta_2$, or $d\Omega$, $d\Omega_1$, $d\Omega_2$.

Differential cross section

$$d\Omega = 2\pi\sin\theta\, d\theta \quad \text{(differential area of annular region)}$$

In the CDM frame

$$d\Omega = 2\pi\sin\theta_1 d\theta_1 = 2\pi|\sin\theta_1| \cdot |\cot\theta_1 d\rho|$$

$$\frac{d\sigma}{d\Omega} = \frac{\rho}{\sin\theta_1}\left|\frac{d\rho}{d\theta_1}\right| = \frac{\rho}{\sin\theta_1}\left|\frac{d\rho}{d\chi}\frac{d\chi}{d\theta_1}\right| \quad \text{(absolute value is being illegal positive)}$$

In the lab frame (for particle 1)

$$d\Omega_1 = 2\pi\sin\theta_1 d\theta_1 = 2\pi|\sin\theta_1| \cdot \left|\frac{d\theta_1}{d\theta_2}\right| \cdot \left|\frac{1 - r^2/r_0^2}{\sqrt{1 - r^2/r_0^2}}\right| d\Omega_2 = \frac{\sin\theta_1}{\cos\frac{\theta_2}{2}}\left|\frac{1 - r^2/r_0^2}{\sqrt{1 - r^2/r_0^2}}\right| d\Omega_2$$

which implies

$$\frac{d\sigma_1}{d\Omega_1} = \frac{d\sigma_2}{d\Omega_2}\frac{\cos\frac{\theta_2}{2}}{\sin\theta_1}\left|\frac{\sqrt{1 - r^2/r_0^2}}{1 - r^2/r_0^2}\right| \quad \text{where} \quad d\Omega_1 = 2\pi\sin\theta_1 d\theta_1$$

The same applies for $d\Omega_1$, $d\Omega_2$.

Then we need to be able to substitute expressions like $d\cos\chi/d\cos\theta_1$ and $d\cos\chi/d\cos\theta_2$.

Recall

$$\cos\chi = \left(\frac{2m}{m_1}\right)\cos^2\theta_1 + \sin^2\theta_1 = \left(\frac{2m}{m_2}\right)\cos^2\theta_2$$

and

$$\chi = \pi - 2\theta_1 \quad \Rightarrow \quad \cos\chi = \cos(\pi - 2\theta_1) = -\cos 2\theta_1$$

for which

$$\begin{aligned} d\cos\chi &= d\cos\theta_1 \left[\left(\frac{2m}{m_1}\right)\cos\theta_1 - \frac{\left(1 - \frac{2m}{m_1}\right)\cos\theta_1}{\sqrt{1 - \left(\frac{2m}{m_1}\right)\cos^2\theta_1}}\right] \quad \text{(for } m_1 > m_2\text{)} \\ d\cos\chi &= d\cos\theta_1 \left[\left(\frac{2m}{m_1}\right)\cos\theta_1 + \frac{\left(1 - \frac{2m}{m_1}\right)\cos\theta_1}{\sqrt{1 - \left(\frac{2m}{m_1}\right)\cos^2\theta_1}}\right] \quad \text{(for } m_1 < m_2\text{)} \end{aligned} \tag{1}$$

and

$$d\cos\chi = -4\cos\theta_2 d\cos\theta_2$$

Q: Explain how one can obtain an expression for small-angle scattering starting from the integral equation for ϕ_m.

Recall

$$\phi_m = \int_{r_{min}}^{\infty} \frac{\rho dr/r^2}{\sqrt{1 - U(r)/E - \rho^2/r^2}}$$

$$\chi = \pi - 2\int_{r_{min}}^{\infty} \frac{\rho dr/r^2}{\sqrt{1 - U(r)/E - \rho^2/r^2}}$$

Small angle scattering corresponds to

$$\chi \to 0 \quad \Rightarrow \quad \rho \to \infty$$

We expect ϕ_m to deviate slightly from the $U(r) \to 0$ case of $\phi_m = \pi/2$.

Expand the factor of the latter in the integrand

$$\frac{1}{\sqrt{1 - \frac{U(r)}{E} - \frac{\rho^2}{r^2}}} = \frac{1}{\sqrt{1 - \frac{\rho^2}{r^2}}}\left(1 - \frac{U(r)}{E}\frac{1}{1 - \frac{\rho^2}{r^2}}\right)^{-1/2} \approx \frac{1}{\sqrt{1 - \frac{\rho^2}{r^2}}}\left(1 + \frac{1}{2}\frac{U(r)}{E}\frac{1}{1 - \frac{\rho^2}{r^2}}\right)$$

The first term when evaluated by ρ/r^2 and integrated from r_{min} to ∞ gives $\pi/2$.

The second term when multiplied by ρ/r^2 and integrated from r_{min} to ∞ is also

$$\frac{1}{2E}\int_{r_{min}}^{\infty} \frac{U(r)\rho dr/r^2}{\sqrt{1 - \rho^2/r^2}} = \frac{1}{2E}\int_{r_{min}}^{\infty} \frac{U(r)\rho dr}{r\sqrt{r^2 - \rho^2}}$$

where we have substituted for r and replaced the term r_{min} by ρ in the upper limit of the last substituted integral.

Thus,

$$\phi_m = \frac{\pi}{2} + \frac{1}{2E}\int_{\rho}^{\infty} \frac{U(r)\rho dr}{r\sqrt{r^2 - \rho^2}} \quad \Rightarrow \quad \chi = -\frac{1}{E}\int_{\rho}^{\infty} \frac{U(r)\rho dr}{r\sqrt{r^2 - \rho^2}}$$

Now the integral

$$I = \int_{\rho}^{\infty} \frac{U(r)dr}{r\sqrt{r^2 - \rho^2}}$$

can be integrated by parts writing

$$u = U(r), \quad dv = \frac{dr}{r\sqrt{r^2 - \rho^2}}$$

for which

$$du = \frac{dU}{dr}dr, \quad v = \frac{1}{\rho}\sec^{-1}\left(\frac{r}{\rho}\right)$$

where the last result was obtained making the substitution $u = r^2 - \rho^2$ in the integral for v.

Thus,

$$I = \frac{U(r)}{\rho}\sec^{-1}\left(\frac{r}{\rho}\right)\Bigg|_{\rho}^{\infty} - \int_{\rho}^{\infty} \frac{dU}{dr}\frac{1}{\rho}\sec^{-1}\left(\frac{r}{\rho}\right)dr$$

where the first term vanishes assuming $U(r) \to 0$ faster than $1/r$ as $r \to \infty$.

Substituting I back into the expression for ϕ_m gives

$$\chi = \frac{1}{E}\int_{\rho}^{\infty} \frac{dU}{dr}\sec^{-1}\left(\frac{r}{\rho}\right)dr = \frac{1}{E}\int_{\rho}^{\infty} \left(\frac{d}{dr}\frac{U}{\rho}\sec^{-1}\left(\frac{r}{\rho}\right)\right)dr$$

which is the desired result.

6. Small oscillations (21-23)

Q: Explain what stable equilibrium means in terms of the potential energy $U(q)$.

Stable equilibrium means there exists a local minimum at some q_0

$$\left.\frac{dU}{dq}\right|_{q_0} = 0, \quad \left.\frac{d^2U}{dq^2}\right|_{q_0} > 0$$

Q: Calculate the frequency for small oscillations about a position of stable equilibrium.

Lagrangian

$$L = \frac{1}{2}m\dot{q}^2 - U(q)$$

Let q_0 be a position of stable equilibrium, and define

$$\eta = q - q_0$$

which implies $\dot{\eta} = \dot{q}$.

Then for small deviations around q_0

$$U(q) = U(q_0) + \left.\frac{dU}{dq}\right|_{q_0}\eta + \frac{1}{2}\left.\frac{d^2U}{dq^2}\right|_{q_0}\eta^2 + \cdots = U_0 + \frac{1}{2}k\eta^2$$

where

$$U_0 = U(q_0), \quad k = \left.\frac{d^2U}{dq^2}\right|_{q_0}$$

So for small deviations around q_0

$$L = \frac{1}{2}m\dot{\eta}^2 - \frac{1}{2}k\eta^2 - U_0$$

where $\eta = x(q)$ and we have dropped the constant U_0 from the Lagrangian

Lagrange's equation

$$\ddot{\eta} = -\left(\frac{m}{k}\right)\eta = -\omega^2\eta$$

gives

$$\omega_0 = \sqrt{\frac{k}{m}}$$

which the general solution

$$\eta = \alpha\cos(\omega_0 t) + \alpha\sin(\omega_0 t) \quad \Rightarrow \quad q = q_0 + \alpha\cos(\omega_0 t) + \alpha\sin(\omega_0 t)$$

Q: Solve the equations of motion for both free and forced oscillation in one dimension, noting the difference between the general solution of the homogeneous equation and a particular integral of the inhomogeneous equation.

From the previous part we have that the EOM for free oscillations is

$$\ddot{\eta} + \omega_0^2\eta = 0$$

which has general solution

$$\eta = \alpha\cos(\omega_0 t) + \alpha\sin(\omega_0 t) \quad \Rightarrow \quad \eta = \alpha e^{i\omega_0 t} + \alpha e^{-i\omega_0 t}$$

The solution can also be written as

$$\eta = \alpha\cos(\omega_0 t - \alpha)$$

where

$$\alpha = \sqrt{\alpha^2 + \alpha^2}, \quad \tan\alpha = \alpha/\alpha$$

or as the real part of a complex solution

$$\eta = \alpha e^{i\omega_0 t}, \quad \alpha = \alpha e^{-i\alpha}$$

Forced oscillations

$$\ddot{\eta} + \omega_0^2\eta = f(t)$$

or, equivalently,

$$\ddot{x} + \beta\dot{x} + \omega_0^2 x = f(t)$$

where $\beta = \sqrt{k/m}$.

Then 2nd order ODE for $x(t)$ can be converted to a 1st order ODE by defining

$$\xi = \dot{x} + \lambda x$$

for which

$$\dot{\xi} = \ddot{x} + \lambda\dot{x}$$

and

$$\ddot{\xi} = \dddot{x} - \frac{\omega_0^2}{\lambda}\dot{x}$$

Then a linear 1st order ODE for $\xi(t)$ comes to

$$\dddot{x} + \beta\ddot{x} + \omega_0^2\dot{x} = \dot{f}(t)$$

which we can rewrite in differential notation as

$$d\xi(t) = f(t)dt - (\beta\xi)dt + \lambda\xi$$

Although the LHS is not an exact differential, it can be made so by multiplying by an integrating factor $\mu(t)$ for which

$$\mu(t)d\xi + \mu(t)\beta\xi dt - \lambda\mu(t)\xi dt = \mu f$$

for some function $\xi(t,\mu)$. The integrating factor $\mu(t)$ can be found by setting

$$\frac{\partial\xi}{\partial t} = \mu f - \mu\beta\xi + \lambda\mu\xi, \quad \frac{\partial\xi}{\partial\mu} = \mu\xi(t)$$

where

$$\frac{\partial^2\xi}{\partial\mu\partial t} = f - \beta\xi + \lambda\xi, \quad \frac{\partial^2\xi}{\partial t\partial\mu} = \mu\dot{\xi} + \mu\xi$$

which is a consequence of

$$\frac{\partial^2\xi}{\partial\mu\partial t} = \frac{\partial^2\xi}{\partial t\partial\mu} \quad \text{with} \quad \frac{\partial\xi}{\partial t} = \mu f(t) - \mu\beta\xi + \lambda\mu\xi, \quad \frac{\partial\xi}{\partial\mu} = \mu\xi(t)$$

leading to

$$\mu\dot{\xi} = f - \beta\xi + \lambda\xi \quad \Rightarrow \quad \dot{\xi} = \frac{f}{\mu} - (\beta - \lambda)\xi$$

So from ξ we solve

$$\dot{x} + \lambda x = \xi$$

for the solutions to the 2nd equation to

$$\dot{x} + \lambda x = \xi$$

for either function $\chi(t)$.

The function $\chi(t)$ is determined by substituting this solution for ξ back into the 1st equation

$$\dot{x}(t) + \chi'(t) - \lambda\chi(t) + \beta\chi(t) = f(t)$$

Subtracting out previous solution for $\chi(t)$ leads to

$$\dot{x}(t) = -\lambda x(t) + \chi(t)$$

which implies

$$\chi'(t) = \int e^{-\lambda t} f(t) dt$$

Thus,

$$\chi(t) = \int e^{\lambda t} dt \int e^{-\lambda t} f(t) dt$$

The solution to the original 1st order ODE for y is then given by $\xi = \dot{x} + \lambda x$ as

$$\dot{x} + \lambda x = \int e^{\lambda t} dt \int e^{-\lambda t} f(t) dt$$

Returning to the differential equation for $\chi(t)$, we see that χ_1 obey the rule of $\chi'(t)$ and $\chi(t)$ obey the rule of $\chi'_1(t)$. Thus, the solution for $\chi(t)$ is given by

$$\chi(t) = \int e^{\lambda t} dt \int e^{-\lambda t} f(t) dt + \alpha\chi_1(t) + \alpha$$

By choosing the limits on the integrals to run from 0 to t, the constant terms α, α vanish, leaving

$$\boxed{\chi(t) = \int_0^t dt \int_0^t e^{-\lambda t} f(t) dt + \alpha\chi_1(t)}$$

The first term on the RHS is a particular solution $\chi_p(t)$ to the differential equation for $\xi(t)$, the second term is the general solution to the homogeneous equation and involves the arbitrary constant α.

To return to $x(t)$, we recall the definition

$$\xi = \dot{x} + \lambda x$$

which implies

$$\dot{x} + \lambda x = \int e^{\lambda t} dt \int e^{-\lambda t} f(t) dt + \alpha\chi_1(t) + \alpha$$

NOTE: The same solution for $\chi(t)$ can be obtained if we instead substitute our ansatz from

$$\chi(t) = \lambda x e^{\lambda t}$$

for which a particular solution of the differential equation $\dot{\chi} - \lambda\chi = f(t)$ is to have

$$\dot{\chi} - \lambda\chi = \lambda\dot{x}e^{\lambda t} + \lambda\dot{x}e^{\lambda t} - \lambda^2 x e^{\lambda t} - \lambda^2 x e^{\lambda t} = f(t)$$

Note that we added the term $\alpha\chi_1(t)$ because it is a solution of the homogeneous equation as $\dot{\chi}_1 - \lambda\chi_1 = 0$.

By Duhamel's theorem, the most general $f(t)$ is superposition of impulse forces

$$f(t) = \int_0^t f(\tau)\delta(t - \tau)d\tau$$

which means that a particular solution for the most general $f(t)$ is superposition of particular solutions for impulse forces

$$\chi_p(t) = \int_0^t d\tau \int_0^t e^{\lambda t} dt \int_0^t e^{-\lambda t} f(\tau)\delta(t - \tau)d\tau$$

$$\chi_p(t) = \int_0^t d\tau \int_0^t e^{\lambda t} dt \int_0^t e^{-\lambda t} f(\tau)\delta(t - \tau)d\tau \quad \Rightarrow \quad \chi_p(t) = \int_0^t d\tau \int_\tau^t e^{\lambda t} dt \int_\tau^t e^{-\lambda t} f(\tau)d\tau$$

Next swap the order of the integrals that gives

$$\chi_p(t) = \int_0^t d\tau \int_\tau^t e^{\lambda t} dt \int_\tau^t e^{-\lambda t} f(\tau)d\tau \quad \Rightarrow \quad \chi_p(t) = \int_0^t d\tau \int_\tau^t e^{\lambda(t-\tau)} dt \int_\tau^t e^{-\lambda(t-\tau)} f(\tau)d\tau$$

which is the symbolic solution we found earlier.

Calculate the normal-mode frequencies and normal-mode solutions for small oscillations of systems with more than one DOF.

The Lagrangian

$$L = \frac{1}{2}\sum_{ij}(a_{ij}\dot{q}_i\dot{q}_j - V_{ij}q_i q_j)$$

becomes

$$L = \frac{1}{2}\sum_{ij}a_{ij}\dot{q}_i\dot{q}_j - \frac{1}{2}\sum_{ij}V_{ij}q_i q_j$$

for small oscillations around q_0, where

$$a_{ij} = \left.a_{ij}\right|_{q_0}, \quad V_{ij} = \left.\frac{\partial^2 V}{\partial q_i \partial q_j}\right|_{q_0}$$

Lagrange's equations

$$\sum_j a_{ij}\ddot{q}_j + \sum_j V_{ij}q_j = 0, \quad i = 1, 2, \cdots, n$$

We guess a sinusoidal solution of the form

$$q_j = \alpha_j e^{i\omega t}, \quad i = 1, 2, \cdots, n$$

which converts the above ODEs to

$$-\omega^2\sum_j a_{ij}\alpha_j + \sum_j V_{ij}\alpha_j = 0, \quad i = 1, 2, \cdots, n$$

or, equivalently,

$$\sum_j (V_{ij} - \omega^2 a_{ij})\alpha_j = 0, \quad i = 1, 2, \cdots, n$$

These equations have a non-trivial solution for the α_j only if the matrix $V_{ij} - \omega^2 a_{ij}$ is non-invertible.

Thus, we must have

$$\boxed{\det|V_{ij} - \omega^2 a_{ij}| = 0 \quad \text{(eigenvalue equation)}}$$

For each ω that solves the above equation, with degenerate principal axes α and α for the plane perpendicular to the twin symmetric axis, one can calculate $\beta = \alpha_1/\alpha_2$ using the following equation

$$\boxed{\sum_j (V_{ij} - \omega^2 a_{ij})\alpha_j = 0 \quad \text{(eigenvector equation)}}$$

7. Rigid body motion (31-36, 38)

Q: Give a diagram showing the body frame and fixed (inertial) reference frame.

Solution:

- (X, Y, Z): inertial frame
- (x_1, x_2, x_3): body frame (non-inertial)
- $\mathbf{R}$: position vector of the CM in the inertial frame
- $\mathbf{r}_i$: position vector of m_i in the body frame (body-based at the CDM of the body)

Q: Show that the angular velocity vector is unchanged under a shift of the origin of the body frame.

Consider a shift of origin of the body frame from $\mathbf{R}$ to $\mathbf{R} - \mathbf{b}$. In the inertial frame nothing moves so the velocities of the particles are not affected.

Nor is the inertial frame

$$\mathbf{v}_i' = \frac{d}{dt}\mathbf{r}_i' + \mathbf{R}' + \mathbf{b}'$$

where $\mathbf{r}_i' = d\mathbf{b}/dt$. Expanding the RHS of the above expression, we have

$$\mathbf{v}_i' = \mathbf{R}' + \mathbf{b}' + \frac{d}{dt}\mathbf{r}_i' = \mathbf{R}' + \mathbf{b}' + \boldsymbol{\omega}\times\mathbf{r}_i' = \mathbf{R}' + \boldsymbol{\omega}\times(\mathbf{r}_i' + \mathbf{b}') = \mathbf{R}' + \boldsymbol{\omega}\times\mathbf{r}_i$$

where

$$\mathbf{b}' + \frac{d}{dt}\mathbf{r}_i' = \mathbf{b}' + \boldsymbol{\omega}\times\mathbf{r}_i' = \boldsymbol{\omega}\times(\mathbf{r}_i' + \mathbf{b}')$$

This means that the angular velocity vector $\boldsymbol{\omega}$ is a property of the rigid body as a whole. It is associated with any particular point in the body.

Q: Write down an expression for the components I_{ij} of the inertia tensor as a sum over discrete mass points or as an integral over the volume of the body.

Discrete mass points:

$$I_{ij} = \sum_\alpha m_\alpha(\mathbf{r}_\alpha^2\delta_{ij} - x_{\alpha i}x_{\alpha j})$$

Continuous mass distribution:

$$I_{ij} = \int_V \rho(\mathbf{r})(\mathbf{r}^2\delta_{ij} - x_i x_j)dV$$

where we have simply replaced m_α by $\rho(\mathbf{r})dV$ and the summation by an integral.

Q: Indicate how the components of the inertia tensor change if one shift the origin of the body frame.

Consider a shift of the origin of the body frame from the CM to some point $\mathbf{a}$. Let the position of body parts in on the CDM and the position of its on this origin $\mathbf{r}_\alpha$. Then

$$\mathbf{r}' = \mathbf{r} + \mathbf{a}$$

So where

$$I_{ij} = \sum_\alpha m_\alpha(\mathbf{r}_\alpha'^2\delta_{ij} - x_{\alpha i}'x_{\alpha j}') = \sum_\alpha m_\alpha[(\mathbf{r}_\alpha + \mathbf{a})^2\delta_{ij} - (x_{\alpha i} + a_i)(x_{\alpha j} + a_j)]$$

$$I_{ij} = \sum_\alpha m_\alpha(\mathbf{r}_\alpha^2\delta_{ij} - x_{\alpha i}x_{\alpha j}) + \sum_\alpha m_\alpha(\mathbf{a}^2\delta_{ij} - a_i a_j) - \sum_\alpha m_\alpha(x_{\alpha i}a_j + a_i x_{\alpha j})$$

$$I_{ij} = I_{ij}' + \sum_\alpha m_\alpha(\mathbf{a}^2\delta_{ij} - a_i a_j) - \sum_\alpha m_\alpha(x_{\alpha i}a_j + a_i x_{\alpha j})$$

Thus

$$\boxed{I_{ij} = I_{ij}' + M(\mathbf{a}^2\delta_{ij} - a_i a_j)}$$

The parallel axis theorem is a special case of the above general result when the origin of the body frame is set to be defined as $I'(\mathbf{r}) = \sum_\alpha m_\alpha r_\alpha$.

Q: Obtain or identify the principal axes of inertia for various rigid bodies.

Principal axes correspond axes x_1, x_2, x_3 whereby through the CDM of the body the inertia tensor is diagonal.

$$I_{ij} = I_i\delta_{ij}$$

Principal axes always agree with symmetry axes of the body, if they exist.

If the rigid body owns such symmetry, one can always diagonalize I_{ij} directly, which is by finding the eigenvectors and eigenvalues of the matrix I_{ij}. The eigenvalues are the principal moments of inertia, the eigenvectors are the principal axes.

Q: Calculate the principal moments of inertia for various rigid bodies.

One can use the above expressions to calculate the principal moments of inertia for various rigid bodies consisting of either discrete mass points or for continuous mass distributions. Below are the principal moments of inertia for various bodies:

Straightforward since in that right-base has uniform mass distribution, and the CDM is at the origin, so a moment can be just taken at the origin.

One needs to use the volume element appropriate for the geometry of the rod body:

- Cartesian coordinates: $dV = dx\,dy\,dz$ for base objects $M = \rho V = \rho abc$
- Spherical coordinates: dV of for spherical objects or ellipsoids, with the axes approximately rescaled: $dV = r^2\sin\theta\,dr\,d\theta\,d\phi$.
- Cylindrical coordinates: $dV = \rho\,d\rho\,d\phi\,dz$ for cylinders or cones with $M = \rho V = \rho\pi R^2 h$ for a cylinder.

For objects like a cone or a cylinder, with degenerate principal axes α and α in the plane perpendicular to the twin symmetric axis, one can calculate $I = I_1 = I_2$ using the following theorem:

$$I = \int dm\,x^2 = \int dm\,y^2 = \frac{1}{2}\int dm(x^2 + y^2) = \frac{1}{2}\int dm\,\rho^2 = \frac{1}{2}I_3$$

which implies

$$I = \frac{1}{2}\int dm\,\rho^2 = \frac{1}{2}\int \rho\,dV\,\rho^2 = \frac{1}{2}\int \rho\,\rho^2\,dV = \frac{1}{2}\int \rho^3\,dV$$

The attached PDF is:

$$I = I_1 + I_2 = \int_{\mathcal{B}} \rho(x)\|x\|^2 - x^2 + x_3^2 \, dx + \int_{\mathcal{B}} \rho(x)\|x\|^2 - x_1^2 + x_3^2 \, dx + \int_{\mathcal{B}} \rho(x)\|x\|^2 - x_2^2 + x_3^2 \, dx$$

$$I = I_1 + I_2 = \int_{\mathcal{B}} \rho(x)\,2\,\|x\|^2 - \|x\|^2 \, dx$$

where the last integral is often easy to do.

Cylinder:

Applying these results to a uniform cylinder of total mass m_{tot}, height h, and radius R, we find

$$I_1 = I_2 = \int_{\mathcal{B}} \rho(x)\left(\frac{R^2}{2}\right) \, dx = \frac{1}{2} m_{tot} R^2$$

It is interesting to note the following limits:

- $h \to 0$ for a thin disk:

$$I_1 = I_2 = \frac{1}{2} m_{tot} R^2, \quad I_3 = \frac{1}{2} m_{tot} R^2$$

- $R \to 0$ for a thin rod:

$$I_1 = I_2 = \frac{1}{12} m_{tot} h^2, \quad I_3 = 0$$

Cone:

For a cone, it is simplest to first calculate the components of the inertia tensor $\mathrm{w.r.t.}\ x^1, x^2$ axes with the origin at the tip of the cone and the symmetry symmetry axis directed along x^3 the uniform right circular cone of total mass m_{tot}, height h, and base radius R, the base volume of the cone is $\pi \cdot h \cdot R^2/3$. The CDM of mass is located at $x^3 = 3/4 \cdot h$. So we find that

$$I_1 = I_2 = \int_{\mathcal{B}} \rho(x)\left(\frac{R^2}{2}\right) dV = \frac{3}{20} m_{tot} R^2$$

Then use

$$I_3 = I_2 + m_{tot}\left(\frac{3}{4}h\right)^2$$

to transform the components of the inertia tensor w.r.t the principal axes of x^1, x^2 to the principal axes x_3 parallel to the CDM. The final result is

$$I_1 = I_2 = \frac{3}{20} m_{tot} R^2 + \frac{9}{16} m_{tot} h^2, \quad I_3 = \frac{3}{20} m_{tot} R^2$$

7) Calculate the kinetic energy of a rigid body in terms of its CDM motion and rotational kinetic energy.

Kinetic energy of the rigid body is obtained as a collection of discrete mass points as

$$T = \frac{1}{2} \sum_{\alpha} m_\alpha v_\alpha^2$$

where $v_\alpha = \dot{x}_\alpha$ is the inertial frame velocity of m_α in the inertial frame.

Since $x_\alpha = X + x_\alpha$ where $\mathbf{X}$ is the position vector of the CDM and x_α is the position vector of m_α w.r.t the CDM, we have

$$v_\alpha = \dot{X} + \dot{x}_\alpha$$

where $\dot{\mathbf{X}} = \frac{d\mathbf{X}}{dt}$ is the velocity of the CDM w.r.t the inertial frame and $\dot{\mathbf{x}}_\alpha$ is the angular velocity of the rigid body. Note that there is no additional velocity term on the RHS since the inertial velocity v_α is defined w.r.t the rigid body.

Thus,

$$T = \frac{1}{2} \sum_{\alpha} m_\alpha (\dot{X} + \dot{x}_\alpha) \cdot (\dot{X} + \dot{x}_\alpha) = \frac{1}{2} \sum_{\alpha} m_\alpha \dot{X} \cdot \dot{X} + \dot{X} \cdot \sum_{\alpha} m_\alpha \dot{x}_\alpha + \frac{1}{2} \sum_{\alpha} m_\alpha \dot{x}_\alpha \cdot \dot{x}_\alpha = \frac{1}{2} M \dot{X} \cdot \dot{X} + \dot{X} \cdot \sum_{\alpha} m_\alpha \dot{x}_\alpha + \frac{1}{2} \sum_{\alpha} m_\alpha \dot{x}_\alpha \cdot \dot{x}_\alpha$$

The three terms on the RHS are:

1st term:

$$\frac{1}{2} M \dot{X} \cdot \dot{X} = \frac{1}{2} M \|\dot{X}\|^2$$

where $\|\cdot\|_{\mathbb{R}^3}$ is, which is the kinetic energy of the CDM w.r.t the inertial frame.

2nd term:

$$\dot{X} \cdot \sum_{\alpha} m_\alpha \dot{x}_\alpha = \dot{X} \cdot \left(\sum_{\alpha} m_\alpha x_\alpha \right)^{\cdot} = 0$$

Since $\sum_{\alpha} m_\alpha x_\alpha = 0$ by definition of the CDM frame.

3rd term:

$$\frac{1}{2} \sum_{\alpha} m_\alpha \dot{x}_\alpha \cdot \dot{x}_\alpha = \frac{1}{2} \sum_{\alpha} m_\alpha \|\dot{x}_\alpha\|^2$$

Using vector identities

$$\mathbf{A} \cdot (\mathbf{B} \times \mathbf{C}) = \mathbf{B} \cdot (\mathbf{C} \times \mathbf{A}) = \mathbf{B} \mathbf{C} \mathbf{A}$$

and

$$\mathbf{A} \times (\mathbf{B} \times \mathbf{C}) = \mathbf{B}(\mathbf{A} \cdot \mathbf{C}) - \mathbf{C}(\mathbf{A} \cdot \mathbf{B})$$

it follows that

$$(\mathbf{B} \times \mathbf{A}) \cdot (\mathbf{B} \times \mathbf{C}) = (\mathbf{B} \cdot \mathbf{B})(\mathbf{A} \cdot \mathbf{C}) - (\mathbf{B} \cdot \mathbf{C})(\mathbf{A} \cdot \mathbf{B}) = \|\mathbf{B}\|^2 (\mathbf{A} \cdot \mathbf{C}) - (\mathbf{B} \cdot \mathbf{C})(\mathbf{A} \cdot \mathbf{B})$$

so

$$\text{3rd term} = \frac{1}{2} \sum_{\alpha} m_\alpha \|\dot{x}_\alpha\|^2 = \omega \cdot \sum_{\alpha} m_\alpha x_\alpha \times \dot{x}_\alpha + \frac{1}{2} \sum_{\alpha} m_\alpha \|\omega \times x_\alpha\|^2$$

where

$$\dot{x}_\alpha = \frac{d}{dt} x_\alpha = \omega \times x_\alpha$$

Thus, putting all the pieces together:

$$T = \frac{1}{2} M \|\dot{X}\|^2 + \omega \cdot \sum_{\alpha} m_\alpha x_\alpha \times \dot{x}_\alpha + \frac{1}{2} \sum_{\alpha} m_\alpha \|\omega \times x_\alpha\|^2$$

The first term is the translational kinetic energy of the rigid body (its CDM motion), and the second is its rotational kinetic energy about the CDM.

Note that the third term is quadratic in ω and is therefore not a linear term.

The angular momentum of a rigid body is quadratic in the angular velocity and is defined. For rigid body motion it is simpler to define the angular momentum $\mathbf{M}$ of the system not up to the inertial frame origin but instead precisely consulting with the CDM of the rigid body.

In that case

$$\mathbf{M} = \sum_{\alpha} m_\alpha x_\alpha \times \dot{x}_\alpha = \sum_{\alpha} m_\alpha x_\alpha \times \omega \times x_\alpha$$

where x_α is the position vector of mass m_α with respect to the CDM as before.

Since x_α is fixed in the rigid body

$$\dot{x}_\alpha = \omega \times x_\alpha$$

Thus,

$$\mathbf{M} = \sum_{\alpha} m_\alpha x_\alpha \times (\omega \times x_\alpha) = \sum_{\alpha} m_\alpha \left(\|x_\alpha\|^2 \omega - x_\alpha (x_\alpha \cdot \omega) \right)$$

where we used

$$\mathbf{A} \cdot (\mathbf{B} \times \mathbf{C}) = (\mathbf{B} \times \mathbf{C}) \cdot (\mathbf{C} \times \mathbf{A})$$

It is more informative to write this last expression in component notation:

$$M_i = \sum_{\alpha} m_\alpha \left(\|x_\alpha\|^2 \omega_i - x_{\alpha i} \sum_{j=1}^{3} x_{\alpha j} \omega_j \right) = \sum_{\alpha} m_\alpha \left(\|x_\alpha\|^2 \delta_{ij} - x_{\alpha i} x_{\alpha j} \right) \omega_j$$

or

$$\boxed{M_i = \sum_{j=1}^{3} I_{ij} \omega_j}$$

where I_{ij} are the components of the moment of inertia tensor.

8) Write down the equations of motion for a rigid body with respect to an inertial frame.

The EOMs for a rigid body w/ an inertial frame are the force and torque equations:

$$\sum_{\alpha} F_\alpha = \frac{dP}{dt}, \quad \sum_{\alpha} \tau_\alpha = \frac{dL}{dt}$$

where P is the total momentum of the rigid body w/ the inertial frame and $\mathbf{L}$ is angular momentum relative to the CDM. There are no equations because there are 6 DOFs.

Note that $\mathbf{L}$ is not the same as the angular momentum $\mathbf{M}$ about the origin. We want to express $\mathbf{L}$ in terms of the angular velocity ω of the rigid body and the moment of inertia tensor I of the rigid body.

Note that $\mathbf{L}$ and $\mathbf{M}$ are the net external force and torque acting on the body, since the internal forces and torques cancel out by Newton's 3rd law.

One can prove the force and torque equations from different laws:

1st method:

The EOMs can also be obtained from the Lagrangian:

$$L = \frac{1}{2} M \|\dot{X}\|^2 + \frac{1}{2} \sum_{\alpha} m_\alpha \|\omega \times x_\alpha\|^2$$

viewed as a function of the translational and rotational coordinates $\mathbf{X}$ (CDM) and ϕ (Euler angles) and their time derivatives $\dot{\mathbf{X}}$ and $\dot{\phi}$.

Recall

$$\omega = \dot{\phi}$$

where $\mathbf{L}$ $\mathbf{M}$ denotes the time derivative of any vector. $\mathbf{A}$ in the inertial frame and $\mathbf{M}$ denotes the time derivative of the same vector w/r to the body frame. Recall that the time derivatives of a vector w/r to any reference frame is obtained by simply time differentiating the Cartesian components of that vector w/r to that frame, e.g. $(\mathbf{M})_I = dM_i/dt = \dot{M}_i$ $\forall$ i.

Force equations:

$$\mathbf{F} = \frac{d\mathbf{P}}{dt} = M \ddot{\mathbf{X}}$$

Net principal axes

$$\mathbf{F}_i = m\ddot{x}_i, \quad i = 1, 2, 3$$

so that

$$\left(\frac{d\mathbf{P}}{dt} \right)_I = \frac{d\mathbf{P}}{dt} + \omega \times \mathbf{P}, \quad \text{(IR = P)} = \sum_{\alpha} m_\alpha \ddot{x}_\alpha$$

Thus,

$$\begin{aligned} F_1 &= m\left(\ddot{x}_1 - \dot{x}_2\dot{\theta}_3 - \dot{x}_3\dot{\theta}_2\right) \\ F_2 &= m\left(\ddot{x}_2 + \dot{x}_1\dot{\theta}_3 - \dot{x}_3\dot{\theta}_1\right) \\ F_3 &= m\left(\ddot{x}_3 + \dot{x}_1\dot{\theta}_2 - \dot{x}_2\dot{\theta}_1\right) \end{aligned}$$

Torque equations:

$$\mathbf{K} = \frac{d\mathbf{L}}{dt} = \frac{d\mathbf{L}}{dt} + \omega \times \mathbf{M}$$

Net PA principal axes

so that

$$\left(\frac{d\mathbf{L}}{dt} \right)_I = \frac{d\mathbf{L}}{dt} + \omega \times \mathbf{L} = \sum_{\alpha} m_\alpha \dot{x}_\alpha \times \dot{x}_\alpha = 0$$

Thus,

$$\begin{aligned} K_1 &= I_1 \dot{\omega}_1 + (I_3 - I_2)\omega_2\omega_3 \\ K_2 &= I_2 \dot{\omega}_2 + (I_1 - I_3)\omega_1\omega_3 \\ K_3 &= I_3 \dot{\omega}_3 + (I_2 - I_1)\omega_1\omega_2 \end{aligned}$$

11) Draw a diagram showing the definition of the Euler angles (ϕ, θ, ψ).

One needs around $\mathbf{T}$ e.g. to first account for translations $\mathbf{X}$ and define it to the rest of rotate $(\mathbf{T}\mathbf{X}, \mathbf{R})$ and then around the transformed $\mathbf{T}$ axis (which is now the x_3 axis) by ϕ.

Perform Euler angle rotations of body frame

```
In [1]: def Rx(t):
            """Counter-clockwise rotation matrix around x-axis"""
            R = np.zeros((3, 3), dtype=np.float64)
            R[0, 0] = 1.0
            R[1:, 1:] = [[np.cos(t), -np.sin(t)],
                         [np.sin(t), np.cos(t)]]
            return R

In [2]: def Ry(t):
            """Counter-clockwise rotation matrix around y-axis"""
            R = np.zeros((3, 3), dtype=np.float64)
            R[1, 1] = 1.0
            R[[0, 0, 2, 2], [0, 2, 0, 2]] = np.ravel([[np.cos(t), -np.sin(t)],
                                                      [np.sin(t), np.cos(t)]])
            return R

In [3]: def Rz(t):
            """Counter-clockwise rotation matrix around z-axis"""
            R = np.zeros((3, 3), dtype=np.float64)
            R[2, 2] = 1.0
            R[:2, :2] = [[np.cos(t), -np.sin(t)],
                         [np.sin(t), np.cos(t)]]
            return R

In [4]: def Euler(phi, theta, psi):
            """Euler angle rotation matrix"""
            return Rz(psi) @ Rx(theta) @ Rz(phi)

In [5]: def Euler(phi, theta, psi):
            """Euler angle rotation matrix"""
            # Rotation about the z-axis by phi
            R = np.array([[np.cos(phi), -np.sin(phi), 0],
                          [np.sin(phi), np.cos(phi), 0],
                          [0, 0, 1]])
            # Rotation about the x-axis by theta
            R = np.dot(R, np.array([[1, 0, 0],
                                    [0, np.cos(theta), -np.sin(theta)],
                                    [0, np.sin(theta), np.cos(theta)]]))
            # Rotation about the z-axis by psi
            R = np.dot(R, np.array([[np.cos(psi), -np.sin(psi), 0],
                                    [np.sin(psi), np.cos(psi), 0],
                                    [0, 0, 1]]))
            return R

In [6]: # Initialization
        phi = np.pi/4  # 45 degrees
        theta = np.pi/4  # 45 degrees
        psi = np.pi/4  # 45 degrees

        # Get the Euler angle rotation matrix
        R = Euler(phi, theta, psi)

        # Print the result
        print("Euler angle rotation matrix:")
        print(R)

In [7]: # Initialization
        phi = np.pi/4  # 45 degrees
        theta = np.pi/4  # 45 degrees
        psi = np.pi/4  # 45 degrees

        # Get the Euler angle rotation matrix
        R = Euler(phi, theta, psi)

        # Define the vector to be rotated
        v = np.array([1, 0, 0])

        # Rotate the vector
        v_rotated = R @ v

        # Print the result
        print("Rotated vector:")
        print(v_rotated)

In [8]: # Initialization
        phi = np.pi/4  # 45 degrees
        theta = np.pi/4  # 45 degrees
        psi = np.pi/4  # 45 degrees

        # Get the Euler angle rotation matrix
        R = Euler(phi, theta, psi)

        # Define the vector to be rotated
        v = np.array([1, 0, 0])

        # Rotate the vector
        v_rotated = R @ v

        # Print the result
        print("Rotated vector:")
        print(v_rotated)

        # Check if the rotation is correct by applying the inverse rotation
        R_inv = np.linalg.inv(R)
        v_original = R_inv @ v_rotated

        # Print the original vector
        print("Original vector:")
        print(v_original)

In [9]: # Initialization
        phi = np.pi/4  # 45 degrees
        theta = np.pi/4  # 45 degrees
        psi = np.pi/4  # 45 degrees

        # Get the Euler angle rotation matrix
        R = Euler(phi, theta, psi)

        # Define the vector to be rotated
        v = np.array([1, 0, 0])

        # Rotate the vector
        v_rotated = R @ v

        # Print the result
        print("Rotated vector:")
        print(v_rotated)

        # Check if the rotation is correct by applying the inverse rotation
        R_inv = np.linalg.inv(R)
        v_original = R_inv @ v_rotated

        # Print the original vector
        print("Original vector:")
        print(v_original)

        # Check if the rotation is orthogonal
        print("Is the rotation orthogonal?")
        print(np.allclose(R @ R.T, np.eye(3)))

In [10]: # Initialization
         phi = np.pi/4  # 45 degrees
         theta = np.pi/4  # 45 degrees
         psi = np.pi/4  # 45 degrees

         # Get the Euler angle rotation matrix
         R = Euler(phi, theta, psi)

         # Define the vector to be rotated
         v = np.array([1, 0, 0])

         # Rotate the vector
         v_rotated = R @ v

         # Print the result
         print("Rotated vector:")
         print(v_rotated)

         # Check if the rotation is correct by applying the inverse rotation
         R_inv = np.linalg.inv(R)
         v_original = R_inv @ v_rotated

         # Print the original vector
         print("Original vector:")
         print(v_original)

         # Check if the rotation is orthogonal
         print("Is the rotation orthogonal?")
         print(np.allclose(R @ R.T, np.eye(3)))

         # Check if the rotation is proper
         print("Is the rotation proper?")
         print(np.allclose(np.linalg.det(R), 1))

In [11]: # Initialization
         phi = np.pi/4  # 45 degrees
         theta = np.pi/4  # 45 degrees
         psi = np.pi/4  # 45 degrees

         # Get the Euler angle rotation matrix
         R = Euler(phi, theta, psi)

         # Define the vector to be rotated
         v = np.array([1, 0, 0])

         # Rotate the vector
         v_rotated = R @ v

         # Print the result
         print("Rotated vector:")
         print(v_rotated)

         # Check if the rotation is correct by applying the inverse rotation
         R_inv = np.linalg.inv(R)
         v_original = R_inv @ v_rotated

         # Print the original vector
         print("Original vector:")
         print(v_original)

         # Check if the rotation is orthogonal
         print("Is the rotation orthogonal?")
         print(np.allclose(R @ R.T, np.eye(3)))

         # Check if the rotation is proper
         print("Is the rotation proper?")
         print(np.allclose(np.linalg.det(R), 1))

         # Check if the rotation is symmetric
         print("Is the rotation symmetric?")
         print(np.allclose(R, R.T))
```

12) Calculate the components of Ω w/r body frame in terms of the Euler angles and their time derivatives.

From the above diagram, one sees that

$$\Omega = \dot{\phi} + \dot{\theta} + \dot{\psi}$$

$$\dot{\phi} = \dot{\phi}\cos\theta\,\mathbf{e}_3 + \sin\theta\cos\psi\,\mathbf{e}_1 - \sin\theta\sin\psi\,\mathbf{e}_2, \quad \dot{\theta} = \dot{\theta}\cos\psi\,\mathbf{e}_1 - \sin\psi\,\mathbf{e}_2, \quad \dot{\psi} = \dot{\psi}\,\mathbf{e}_3$$

Adding these together we get

$$\Omega = (\dot{\theta}\cos\psi + \dot{\phi}\sin\theta\sin\psi)\,\mathbf{e}_1 + (-\dot{\theta}\sin\psi + \dot{\phi}\sin\theta\cos\psi)\,\mathbf{e}_2 + (\dot{\psi} + \dot{\phi}\cos\theta)\,\mathbf{e}_3$$

with

$$\Omega_1 = \dot{\phi}\sin\theta\sin\psi + \dot{\theta}\cos\psi, \quad \Omega_2 = \dot{\phi}\sin\theta\cos\psi - \dot{\theta}\sin\psi, \quad \Omega_3 = \dot{\phi}\cos\theta + \dot{\psi}$$

13) Solve for the reaction forces for rigid bodies in static equilibrium.

In static equilibrium or rigid body motion, we have the net external forces and torques:

$$\mathbf{F} = \sum_{\alpha} F_\alpha = 0, \quad \mathbf{K} = \sum_{\alpha} \tau_\alpha = 0$$

Given the EOMs for a rigid body, the above equations are equivalent to

$$\mathbf{F} = M\ddot{\mathbf{X}} = 0, \quad \mathbf{K} = \dot{\mathbf{L}} = I\dot{\omega} = 0$$

where the inertial forces are included in the summations over F and τ = 0

Since the EOMs for a rigid body are the translational and rotational velocity, which is at most 6) must equal the number of unknown components of the reaction forces that you are trying to solve for.

8. Non-inertial reference frames (3/9)

1) Draw a diagram making an inertial and non-inertial reference frame.

Notation:

- $\mathcal{F}_0$ = inertial frame
- $\mathcal{F}$ = non-inertial frame
- $\mathbf{x}$ and $\mathbf{v}$ are measured in $\mathcal{F}_0$ in either frame
- $\mathbf{X}$ is the position vector of the origin of $\mathcal{F}$
- $\mathbf{R}$ = position vector of the origin of $\mathcal{F}$ in the non-inertial reference frame

2) Write down the relationship between velocity vectors in inertial and non-inertial reference frames.

Since

$$\mathbf{v}_0 = \mathbf{R} + \mathbf{v}$$

it follows that

$$\mathbf{v}_0 = \dot{\mathbf{R}} + \mathbf{v} + \omega \times \mathbf{r}$$

where $\dot{\mathbf{R}} = \dot{\mathbf{X}}$ and ω is the translational and rotational velocity of $\mathcal{F}$ w.r.t. and is the velocity of $\mathcal{F}$ w.r.t. $\mathcal{F}_0$.

3) Distinguish non-inertial reference frames associated with translational and rotational motion.

- A non-inertial reference frame that undergoes translational motion is called a non-rotating frame or just non-rotating frame. $\omega = 0$ $\dot{\mathbf{R}} = 0$.
- A non-inertial reference frame associated with rotational motion only is known as a rotating frame or simply rotating frame. $\dot{\mathbf{R}} = 0$ but ω is arbitrary.

4) Derive the Coriolis, centrifugal, translational acceleration, and rotational acceleration fictitious force terms.

Recall that

$$\mathbf{v}_0 = \dot{\mathbf{R}} + \mathbf{v} + \omega \times \mathbf{r}$$

Newton's 2nd law in a non-inertial reference frame:

Consider Newton's 2nd law in the non-inertial frame. We want to express $\mathbf{a}_0$ in terms of the acceleration $\mathbf{a}$ in the non-inertial frame plus other terms, which give rise to fictitious forces.

Recall that the time derivative of any vector $\mathbf{A}$ in the non-inertial frame $\mathcal{F}_0$ is given by:

$$\dot{\mathbf{A}}_0 = \frac{d\mathbf{A}}{dt} + \omega \times \mathbf{A}$$

where $\frac{d\mathbf{A}}{dt}$ is the time derivative of $\mathbf{A}$ as the non-inertial frame $\mathcal{F}$. The time derivative of any reference frame is obtained by simply time differentiating the Cartesian components of that vector w/r that frame.

Applying the formula to each part of the velocity vector:

$$\mathbf{v}_0 = \dot{\mathbf{X}} + \mathbf{v} + \omega \times \mathbf{r}$$

Now

$$\mathbf{a}_0 = \frac{d\mathbf{v}_0}{dt}$$

LHS:

$$\mathbf{a}_0 = \frac{d\mathbf{v}_0}{dt}$$

RHS:

$$\frac{d}{dt}\dot{\mathbf{X}} + \mathbf{a} + \frac{d}{dt}(\omega \times \mathbf{r}) = \ddot{\mathbf{X}} + \mathbf{a} + \dot{\omega} \times \mathbf{r} + \omega \times \dot{\mathbf{r}} = \ddot{\mathbf{X}} + \mathbf{a} + \dot{\omega} \times \mathbf{r} + \omega \times (\mathbf{v} + \omega \times \mathbf{r})$$

Thus,

$$\mathbf{a}_0 = \ddot{\mathbf{X}} + \mathbf{a} + \dot{\omega} \times \mathbf{r} + 2\omega \times \mathbf{v} + \omega \times (\omega \times \mathbf{r})$$

Multiplying with $(\mathbf{0})$, the given

$$\mathbf{F} = m\ddot{\mathbf{X}} + m\mathbf{a} + m\dot{\omega} \times \mathbf{r} + 2m\omega \times \mathbf{v} + m\omega \times (\omega \times \mathbf{r})$$

The fictitious forces terms on the RHS are associated with translational acceleration, rotational acceleration, Coriolis, and centrifugal forces.

The inertial equation can also be found from Lagrange's equations starting with the Lagrangian

$$L = \frac{1}{2} m \left(\dot{\mathbf{X}} + \mathbf{v} + \omega \times \mathbf{r} \right)^2 + m\left(\dot{\mathbf{X}} + \mathbf{v} + \omega \times \mathbf{r} \right) \cdot \mathbf{r} - \frac{1}{2} m \|\mathbf{r}\|^2$$

The variance of L w.r.t. $\mathbf{r}$ is

$$\delta L = m\delta\mathbf{r} \cdot \left(\dot{\mathbf{X}} + \mathbf{v} + \omega \times \mathbf{r} \right) + m\delta\mathbf{r} \cdot \left(\mathbf{v} + \omega \times \mathbf{r} \right) - m\delta\mathbf{r} \cdot \mathbf{r}$$

which implies

$$\frac{\partial L}{\partial \mathbf{r}} = m\dot{\mathbf{X}} + m\mathbf{v} + m\omega \times \mathbf{r} + m\omega \times \mathbf{r} + m\omega \times (\omega \times \mathbf{r}) - m\mathbf{r}$$

Lagrange's equations:

$$\frac{d}{dt}\left(\frac{\partial L}{\partial \dot{\mathbf{r}}} \right) = \frac{\partial L}{\partial \mathbf{r}}$$

LHS:

$$\frac{d}{dt}\left(\frac{\partial L}{\partial \dot{\mathbf{r}}} \right) = \frac{d}{dt}\left(m\dot{\mathbf{X}} + m\mathbf{v} + m\omega \times \mathbf{r} + m\omega \times \mathbf{r} \right) = m\ddot{\mathbf{X}} + m\mathbf{a} + m\dot{\omega} \times \mathbf{r} + m\omega \times \mathbf{v} + m\omega \times \mathbf{v} + m\omega \times (\omega \times \mathbf{r})$$

where we used $\mathbf{v} = \dot{\mathbf{r}}$, $\mathbf{a} = \dot{\mathbf{v}}$, $\dot{\omega} = \omega \times \omega = 0$, and $\omega \times (\omega \times \mathbf{r}) = -\omega \times (\mathbf{r} \times \omega)$.

Equating with (0), the given

$$m\ddot{\mathbf{X}} + m\mathbf{a} + m\dot{\omega} \times \mathbf{r} + 2m\omega \times \mathbf{v} + m\omega \times (\omega \times \mathbf{r}) = \mathbf{F}$$

where we use $\mathbf{W} = \dot{\mathbf{W}} + \omega \times \mathbf{W}$ for $\mathbf{W} = \mathbf{R}$ and $\mathbf{r}$.

5) Explain the physical significance of Foucault's pendulum.

The possession of the plane of oscillation of Foucault's pendulum is proof that is still attached to the rotation of the Earth is a non-inertial reference frame.

Reference Frame

Precession of plane of oscillation.

The main contribution to the precession comes from Earth's daily rotational motion. One writes

$$\omega_{\text{Earth}} = 2\pi \text{ rad/day} = \omega$$

for the motion of the pendulum bob in the xy plane, ignoring any terms in the second derivative.

Code for producing the precession motion is given below:

```
In [1]: # Foucault pendulum precession
        # Import necessary modules
        import numpy as np
        import matplotlib.pyplot as plt
        # Set the parameters
        g = 9.81  # acceleration due to gravity
        L = 1.0  # length of the pendulum
        omega = 2*np.pi/24/60/60  # angular velocity of the Earth (one sidereal day)
        phi = np.pi/4  # latitude of the location (in radians)
        # Set the initial conditions
        x0 = 0.1  # initial displacement in the x-direction
        y0 = 0.0  # initial displacement in the y-direction
        vx0 = 0.0  # initial velocity in the x-direction
        vy0 = 0.0  # initial velocity in the y-direction
        # Set the time step and the number of steps
        dt = 0.1  # time step (in seconds)
        n = int(24*60*60/dt)  # number of steps (one sidereal day)
        # Initialize the arrays to store the positions and velocities
        x = np.zeros(n)
        y = np.zeros(n)
        vx = np.zeros(n)
        vy = np.zeros(n)
        x[0] = x0
        y[0] = y0
        vx[0] = vx0
        vy[0] = vy0
        # Integrate the equations of motion using the Euler-Cromer method
        for i in range(1, n):
            ax = -g/L*x[i-1] + 2*omega*vy[i-1]*np.sin(phi)
            ay = -g/L*y[i-1] - 2*omega*vx[i-1]*np.sin(phi)
            vx[i] = vx[i-1] + ax*dt
            vy[i] = vy[i-1] + ay*dt
            x[i] = x[i-1] + vx[i]*dt
            y[i] = y[i-1] + vy[i]*dt
        # Plot the results
        plt.plot(x, y)
        plt.xlabel('x (m)')
        plt.ylabel('y (m)')
        plt.title('Foucault pendulum precession at plane of oscillation')
        plt.show()
```